

RESEARCH PROGRAM TO DEVELOP ALLOYS FOR UP TO 1200°F STRAIN GAGES

BY

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TABLE OF CONTENTS

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- II. OBJECTIVES
- III. PROCEDURE
- IV. GRAPHICAL RESULTS
- V. STRAIN GAGE DESIGN
- VI. STRAIN GAGE EVALUATION
- VII. CONCLUSIONS
- VIII. RECOMMENDATIONS

I. INTRODUCTION

Our rapidly expanding technology has brought forth numerous systems which perform in high-temperature environments. It is necessary to qualify materials for these systems and subsequently evaluate the performance of prototype and production units under operating conditions.

We must be concerned about the effects of temperature on the properties of these materials, especially when resulting changes might jeopardize specified performance of the materials in system components. Of primary concern is temperature dependence of mechanical, physical, metallurgical and electrical properties. The challenge in developing measuring devices and methods to evaluate high-temperature behavior arises from the fact that these devices are themselves subject to the same effects.

In 1957 when the temperature compensation of electric resistance strain gages was first introduced in practical terms, structural evaluation at other than ambient or low temperature conditions became more simple and accurate by an order of magnitude. It became possible to measure static strains accurately up to 600°F, even in the presence of thermal gradients. Soon, however, the development of high

energy power systems and the resulting advent of space exploration placed even greater demands upon measuring devices. One of the most serious needs was for a strain gage which could be used reliably for static measurements above 1000°F. This need has persisted to the present time in the face of considerable development effort which has yielded only partial solutions to the problem.

The essential requirements for a resistance strain gage alloy suitable for the measurement of steady state strains at 1200°F are:

- 1. Metallurgical stability at elevated temperature
- 2. A specific resistance of at least 200 Ohms/CMF
- 3. An apparent strain with temperature no larger than the applied or mechanical strain
- 4. Constant (or linear) temperature coefficient of resistance
- 5. Only moderate change in gage factor with temperature
- 6. Coefficient of expansion (PPM/°F) compatible with high-temperature structural materials
- 7. Only moderate change in gage factor with strain
- 8. Adequate mechanical strength

In order to meet the above requirements, "building blocks" were selected for the design of strain gage alloys (Table I). The investigation reported herein does not exhaust the possibilities for new alloys from this group.

Table I

Elements for Design of Strain Gage Filaments

Element	Atomic Number	Melting Point °F	Resistivity n/CMF	Temperature Coefficient µû/û/°F	Thermal Expansion ps/°F	Modulus of Elasticity 10 ⁶ lb/in ²	Oxidation Temperature °F
A1	13	1220	16	2400	12.9	10	400
11	22	3270	300	3000	4.8	15	500
ಭ	24	3350	7.8	1700	7.0	36	800
Mn	25	2268	260	110-180	12.7	23	70
<u>ር</u> ተ	56	2795	09	3400	η•9	59	009
ဝိ	27	2715	38	3700	8.9	30	575
N	28	2650	50	2700	7.3	30	1100
no	59	1981	11	2200	9.5	16	600
Mo	42	4750	30	1800	2.7	50	400
Pd	94	2830	09	1800	η.9	17	1300
(7.4	6120	33	2500	7.2	53	300
ት ተ	78	3224	59	1700	6.4	ħ Z	2200

II. OBJECTIVES

The present research and development program was undertaken with a threefold purpose:

- 1. Develop satisfactory alloys for temperature compensated strain gages for the measurement of steady-state strains up to 1200°F.
- 2. Critically evaluate these alloys in actual strain gage configurations, taking into consideration necessary refinements in the entire measuring system, e.g., adhesives, lead-in wiring, protective coatings, instrumentation, etc.
- 3. Produce sufficient quantities of these alloys and associated materials to permit fabrication of initial production quantities of gage systems.

III. PROCEDURE

In pursuing the objectives of this investigation, fifteen alloys were melted and wire samples drawn, having diameters of 0.005", 0.002", 0.001". One alloy was reduced to foil having a thickness of 0.0004" and 0.0002".

Pertinent strain gage properties of each of these alloys were determined for various conditions of heat treatment. Three nickel-base "Superalloys" were tested (Table II). The iron-base "Superalloy" evaluated is listed in Table III. A cobalt-base "Superalloy" also was tested (Table IV). Numerous precious-metal alloys of platinum were selected for evaluation (Tables V, VI, and VII).

The alloys selected were vacuum melted and samples were reduced to fine wire and foil by qualified sources. The evaluation of the alloys was conducted at the Detroit facility of William T. Bean, Inc. (Figures 1 and 2) Strain gages were fabricated from each alloy (Figures 2 and 3) and mounted on test specimens (Figure 4).

An improved ceramic cement (H-1) was used as the bonding agent. Nichrome ribbons were used to connect the strain gage filament to lead-in wires. All connections were spot-welded. Stainless steel-clad copper wires with fiberglas insulation were used in the conventional 3-wire

circuit. The completed installation was coated with a white protective coating (Gagekote # 1) in order to reduce radiation effects at elevated temperature. The test specimen was wrapped in several layers of thin fiberglas cloth in order to assure uniform heating and cooling.

Test results are summarized in Tables II through VI. Significant characteristics are graphically presented in this report by the extensive use of an X-Y Recorder, for example, the Resistance vs. Temperature Curves shown in Figure 5.

The E.M.F. of a chromel/alumel thermocouple was used to drive the X-Axis of the Moseley Recorder. The thermocouple output was simultaneously monitored by a Doric DVM.

Table II

Nickel-Base Alloys

Notes	Not stable	Not stable	Not stable	Not stable
_	×	ž	ž	N
Apparent us/°F	19	15-16	17	7-20
µa/a/°F	0 η	32-36	О †	15-45
% AR/100°F	ή.Ο	0.32-0.36	₩.0	0.15-0.45
% AR @ 1100°F	O• 17	3.2-3.6	0.4	1.5-4.5
Gage Factor	2.1	2.5	2.3	2.3
a/CMF @ 100°F	650	662-771	606-755	710-816
. Alloy	Nichrome V 80 Ni 20 Cr	Inconel 102 67 Ni 15 Cr 8 Fe 3 Mo 3 W	Hastelloy N 67 N1 17 Mo 7 Cr 5 Fe	Rene 41 54 N1 19 Cr 10 Mo 3 T1
No.	16	1 2	&	ru.

Table III

	Notes	Not stable
	Apparent us/oF	85
	µа/а/°F	205
Iron-Base Alloy	% AR/100°F	2.05
Irc	% AR @ 1100°F	20.5
	Gage Factor	2°.
	0/CMF @ 100°F	591-625
	Alloy	N-155 30 Fe 21 Cr 20 N1 20 Co
	No.	6

Table IV

Cobalt-Base Alloy

Table V

	Notes	Not stable	Some instability above 1000°F	Not stable	Some instability above 1000°F	Unstable above 1000°F
	Apparent µc/°F	125	7.1	i i	ဗ	ļ
	µΩ/Ω/°F	250	150	20	200	220
of Platinum-Copper	% AR/100°F	2.5	1.5	ŗ.	2.0	8
Alloys of Plat	% AR @ 1100°F	25	15	ſν	50	55
4 l	Gage Factor	2.0	2.1	ole ole	ત 4	o. 1 e
	a/CMF @ 100°F	220-340	†††-0††	Not workable	320-344	Not workable
	Alloy	80 Pt 20 Cu	80 Pt 15 Cu 5 Ni	80 150 Pt 57 Ct 8 k	90 Pt 8 Cu 8 Ku	90 50 PF 8 Ct
	No.	н	15	10	α	12

Table VI

Alloys of Platinum-Nickel

Table VII

Alloys of Platinum-Tungsten

Notes	Good stability to 1400°F	Not stable above	Good stability to 1400°F
Apparent us/°F	0η	83	162
µ2/2/°F	210	200	089
\$ AR/100°F	2.1	2.0	89.
% AR @ 1100°F	21	20	89
Gage Factor	5.3	۲. ۵	ਪ ਜ
a/cmf e 100°F	330-355	320-344	188-210
Alloy	92 Pt 8 ¥	90 Pt 8 & Cu	90 Pt 2 W 8 Ni
No.	13	N	m

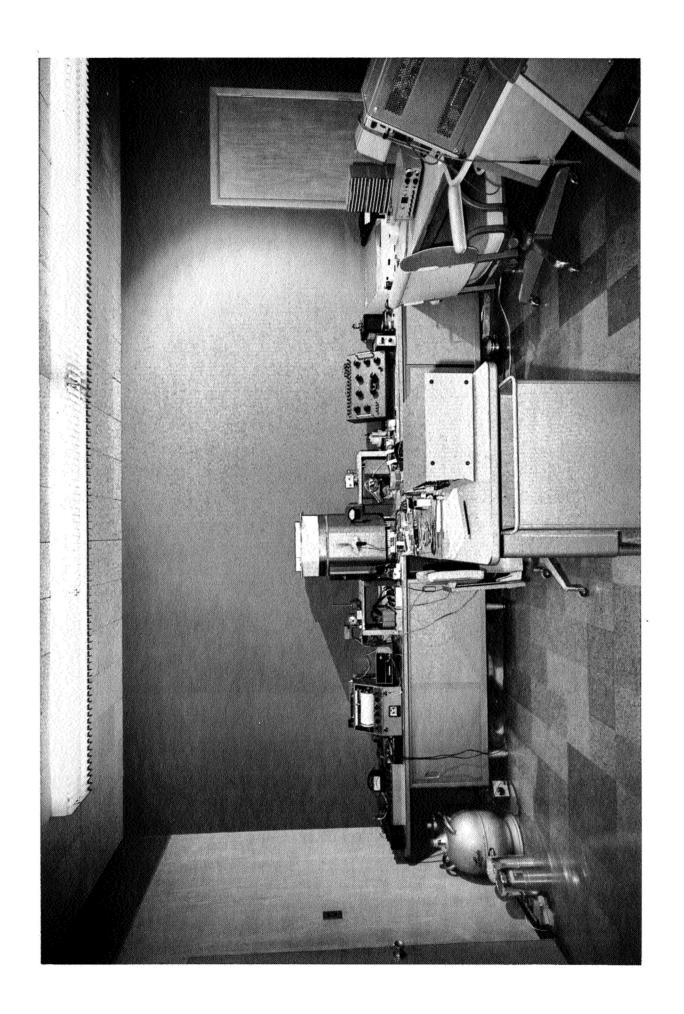


FIGURE 1. STRAIN GAGE EVALUATION LABORATORY



FIGURE 2. STRAIN GAGE FABRICATION & INSTALLATION AREA

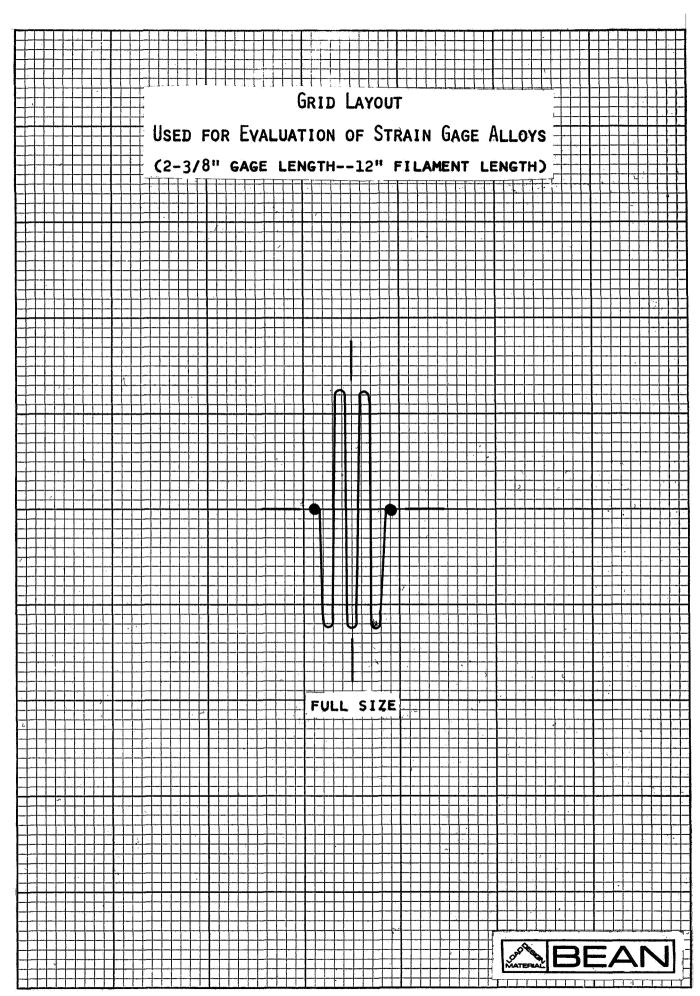
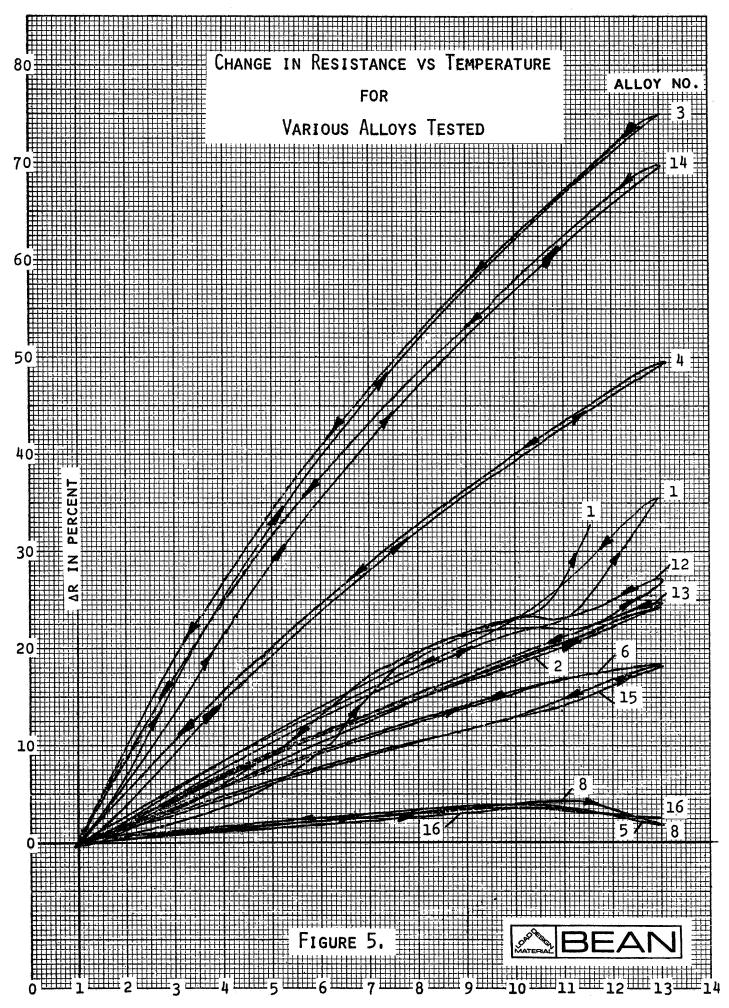


FIGURE 3.

FIGURE 4.

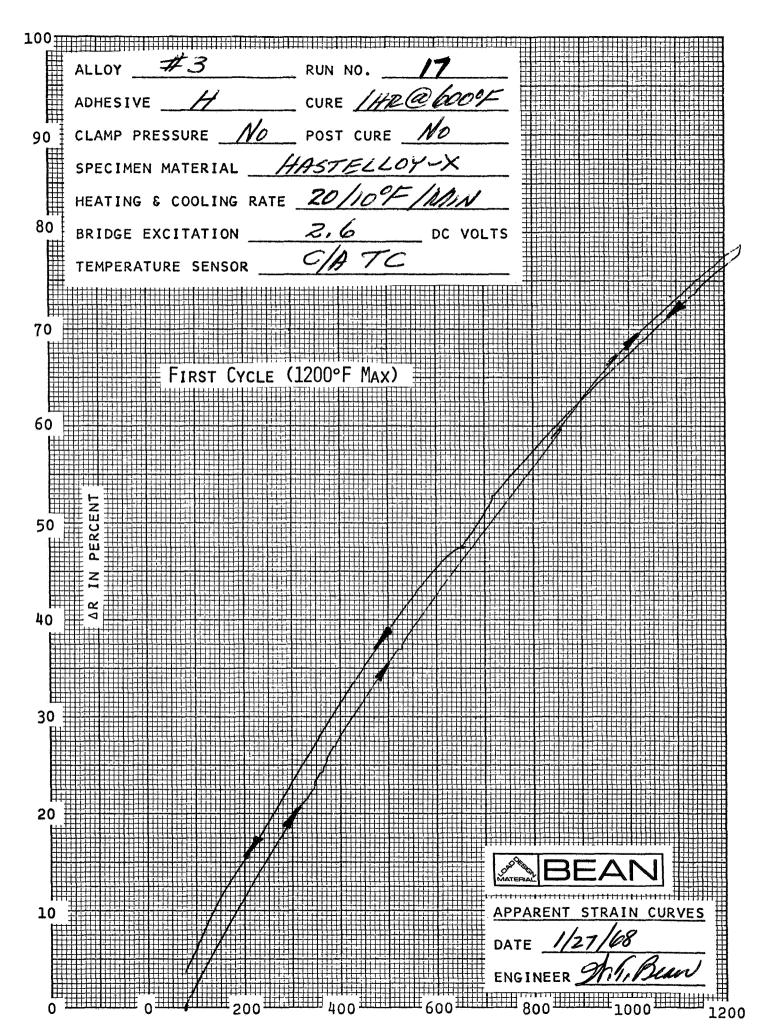


IV. GRAPHICAL RESULTS

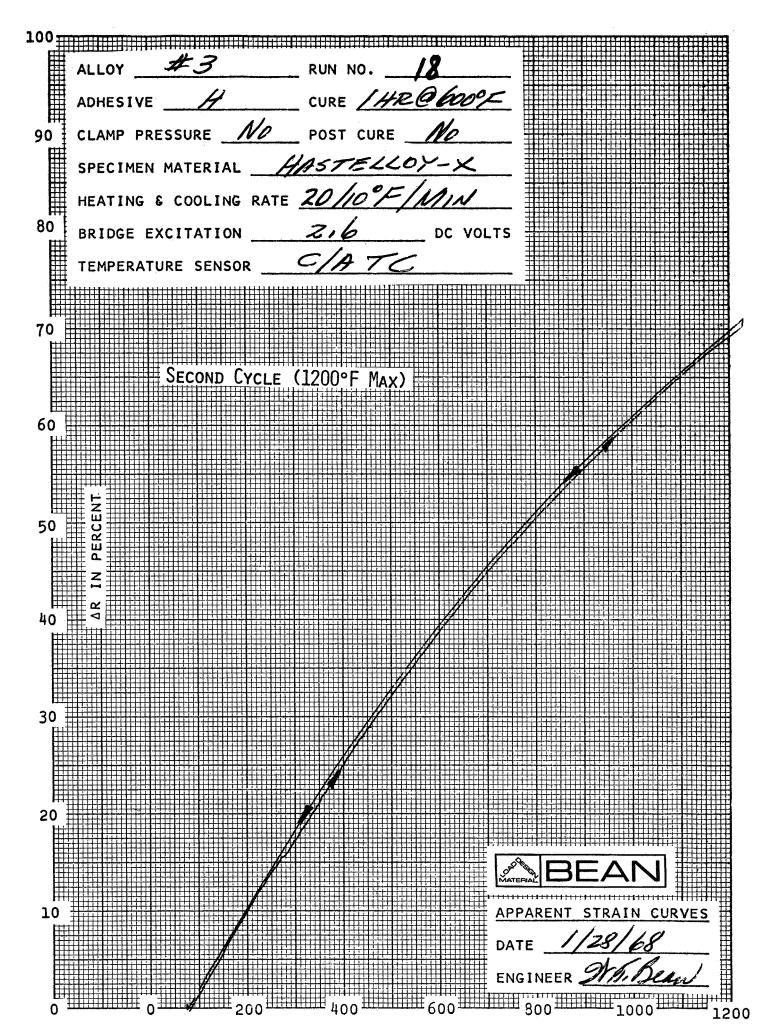
Of all the strain gage materials tested, only three alloys of platinum exhibited satisfactory stability up to 1200°F. Curves showing the first and second heat cycles to 1200°F for these alloys follow (Runs # 17, # 18, # 20, # 21, # 100, # 101). Typical Resistance/Temperature/Time Curves on a high strength nickel-base alloy are shown (Runs # 23, # 27, # 29, # 62, # 160, # 161, # 163 through # 167). Figure 6 combines Runs # 60 and # 61 and indicates the apparent strain from -320°F to +950°F.

Test results on the other alloys follow:

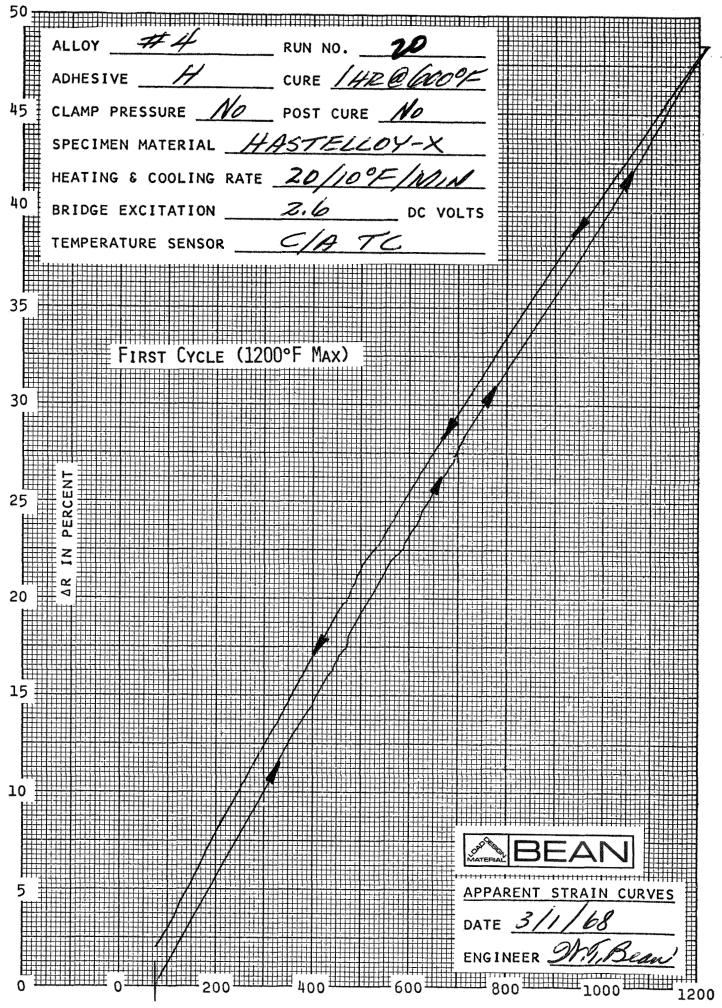
Alloy No.	Run No.
1	9, 10
2	13, 14, 15
5	24, 60
6	84, 85
7	88, 89
8	91, 92
9	94, 95
10	97
11	102, 104
14	107
15	109

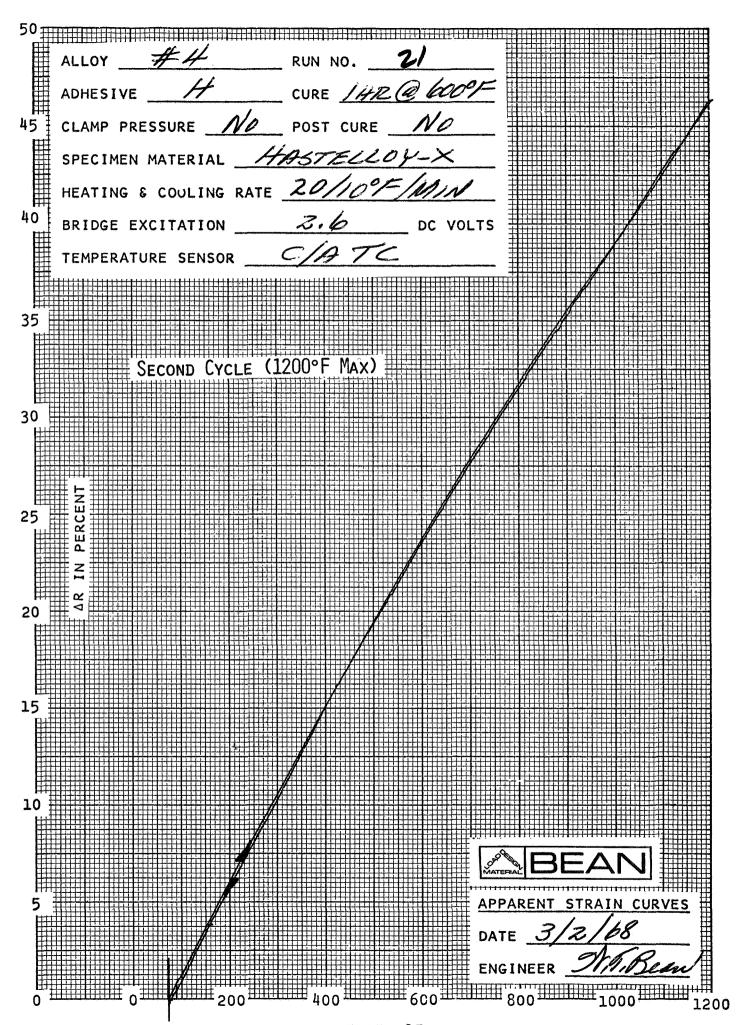


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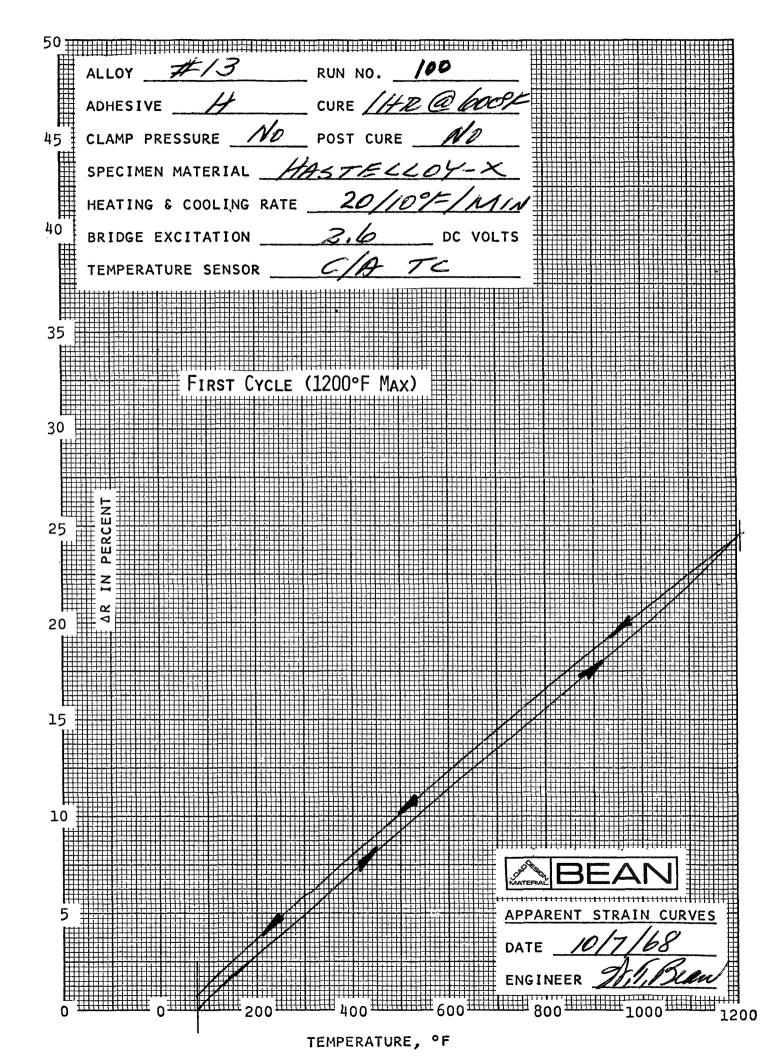


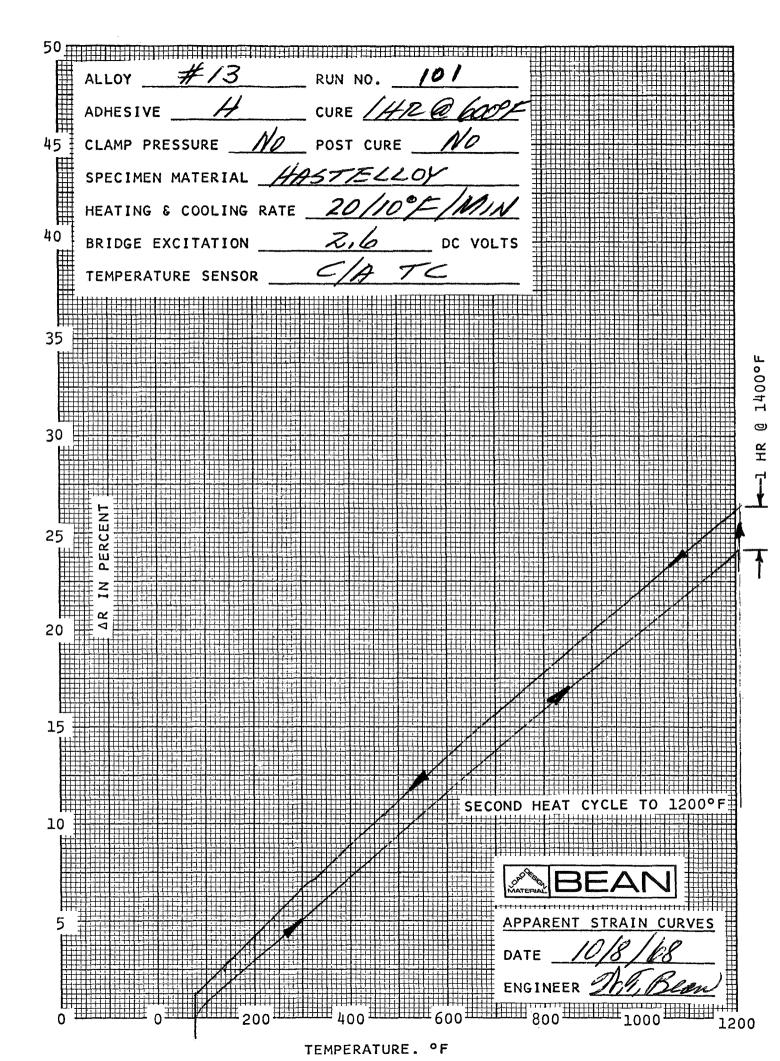
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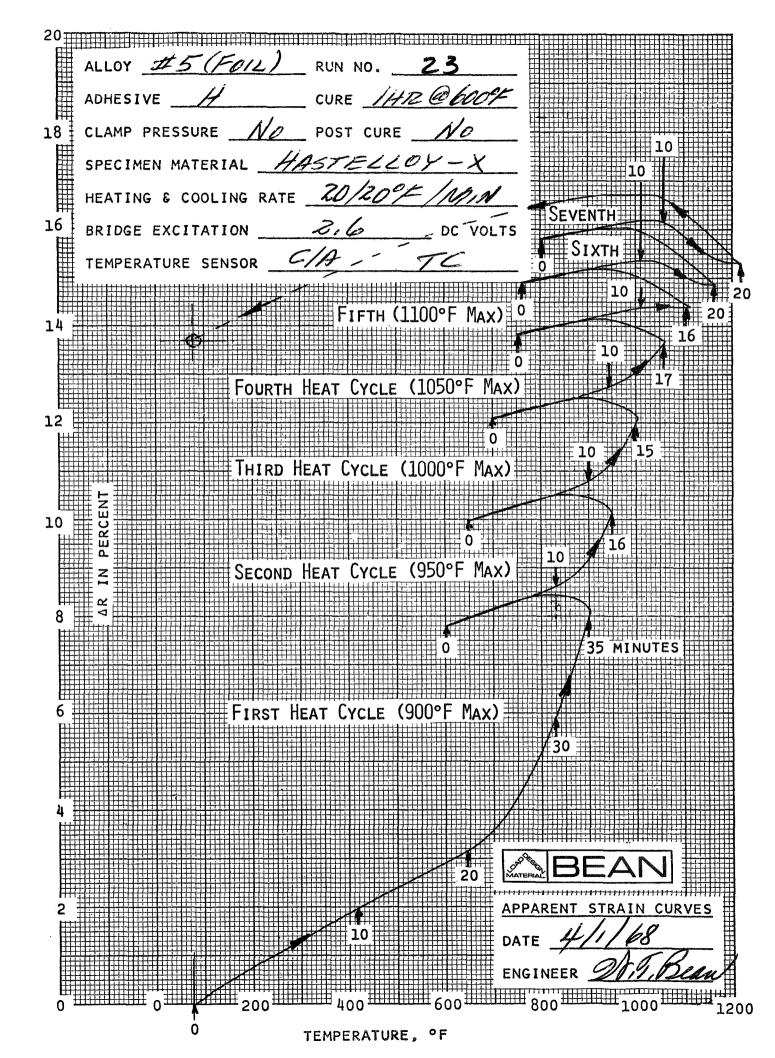


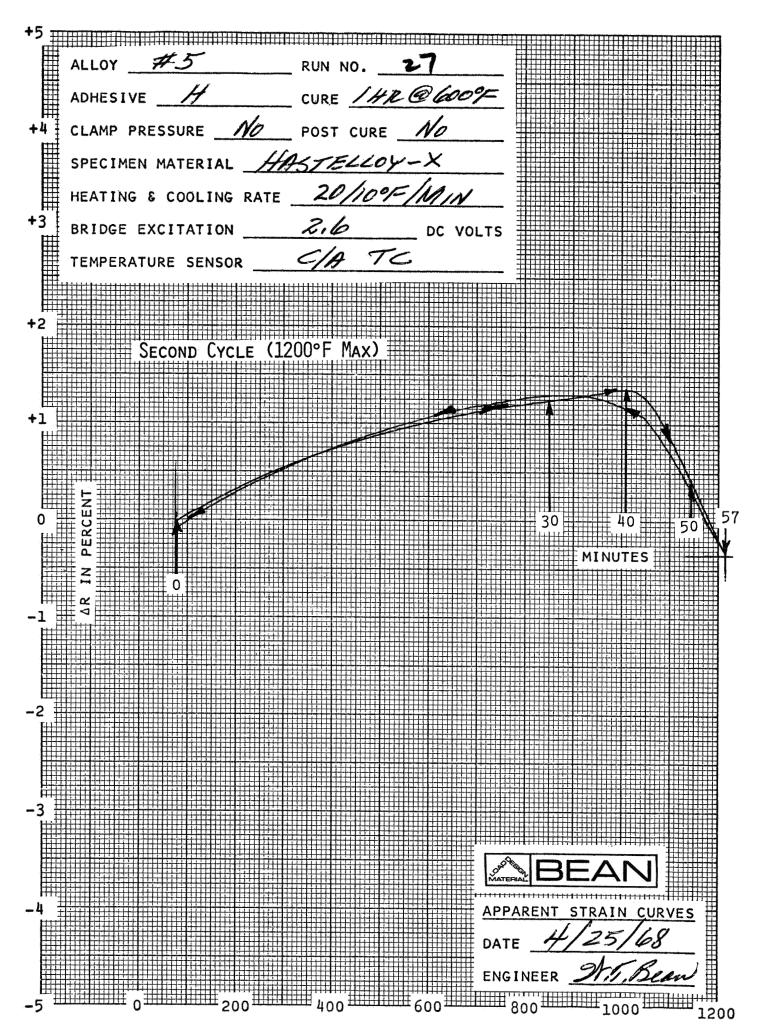


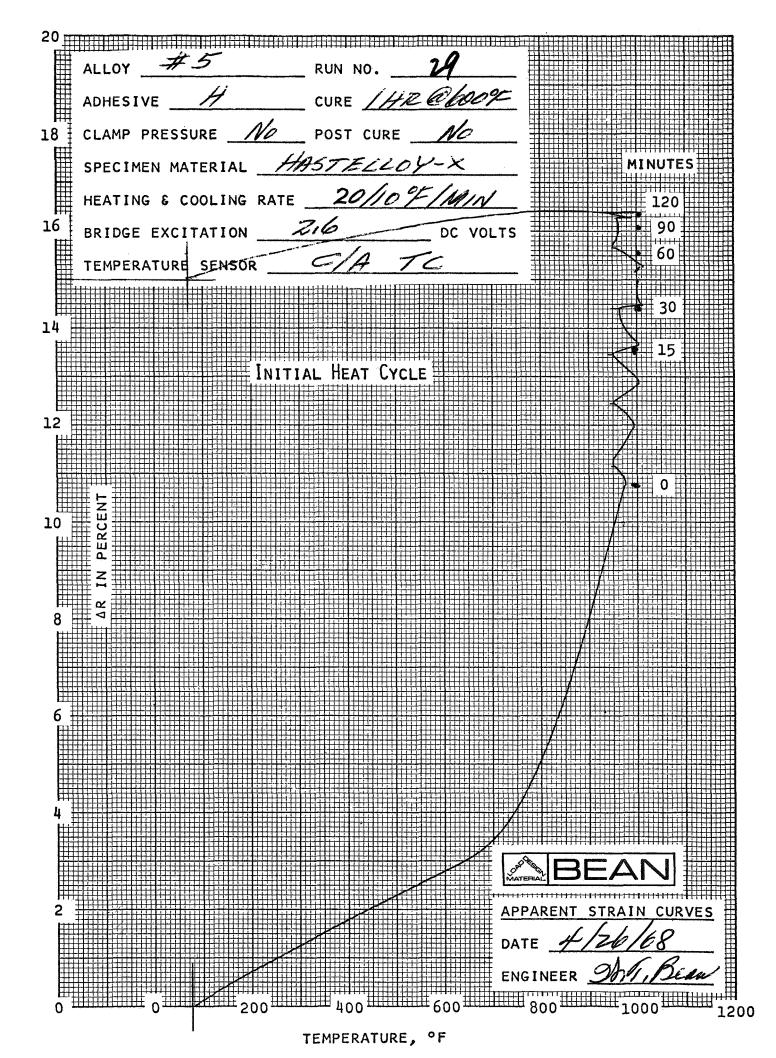
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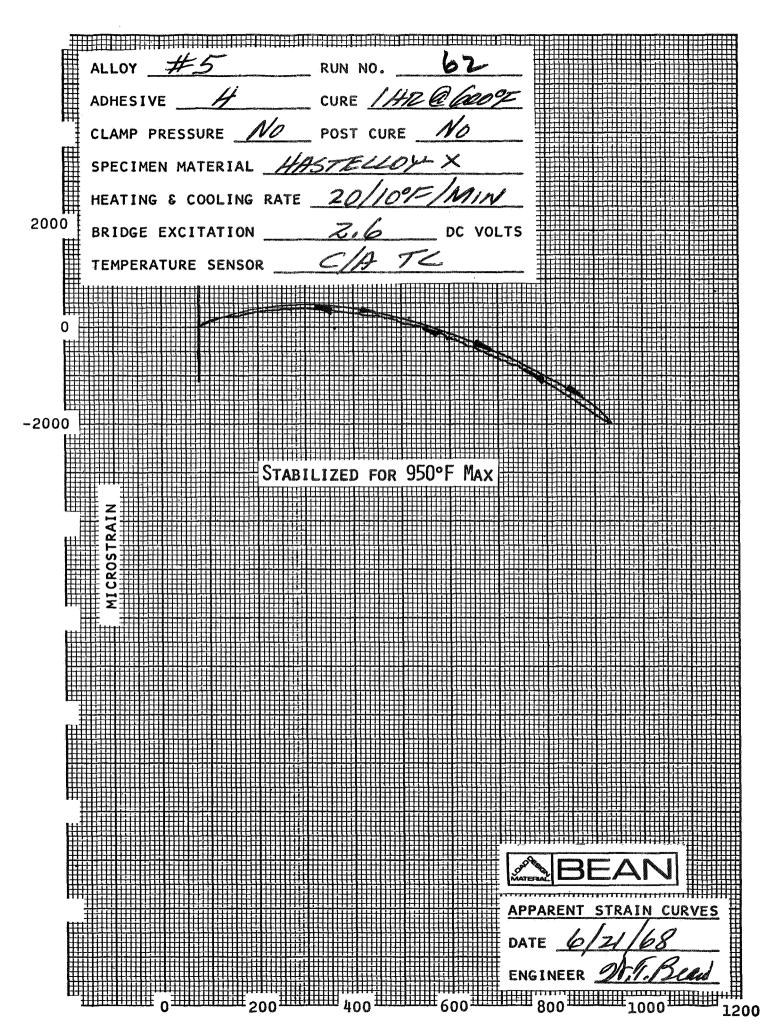


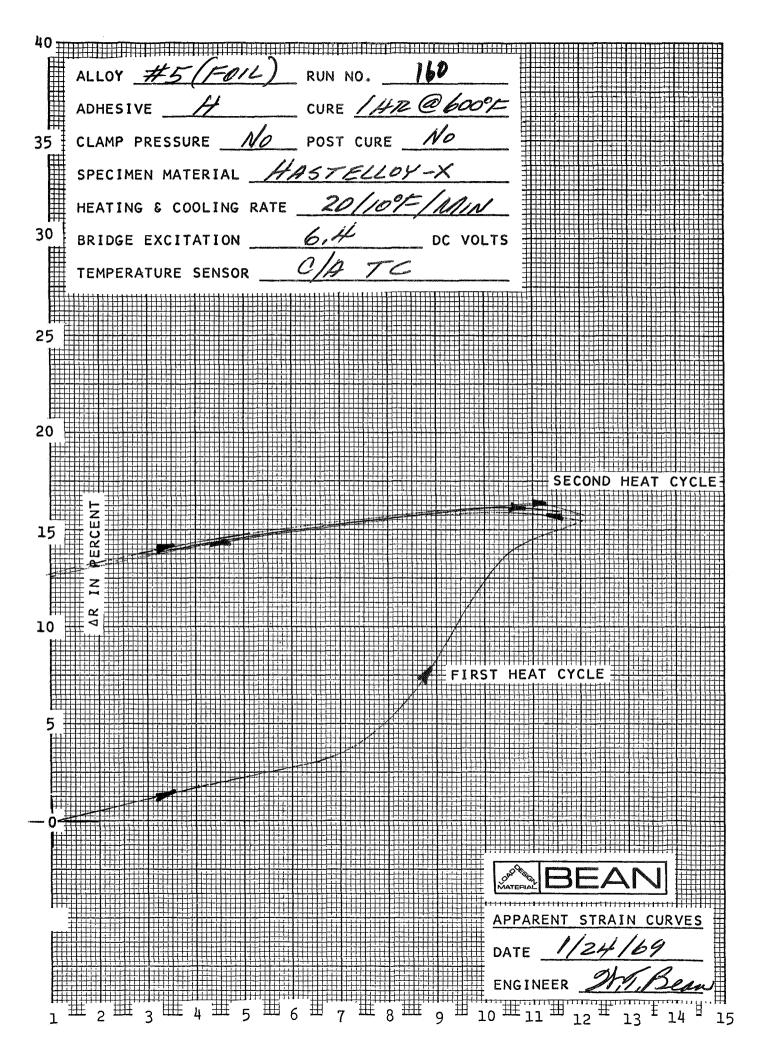




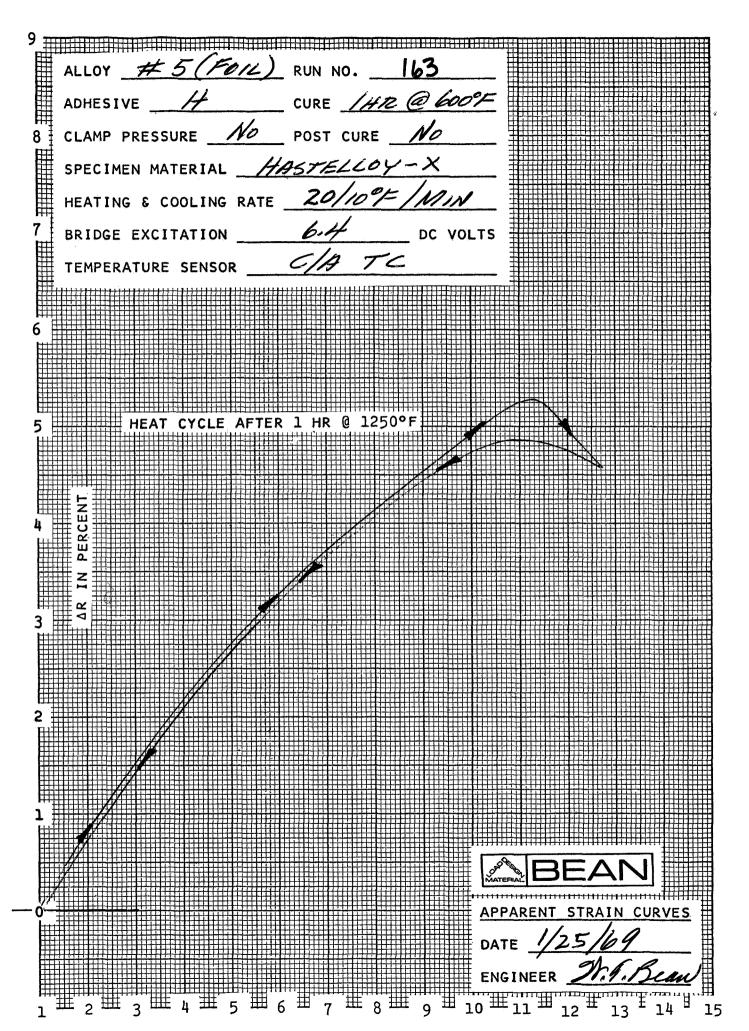


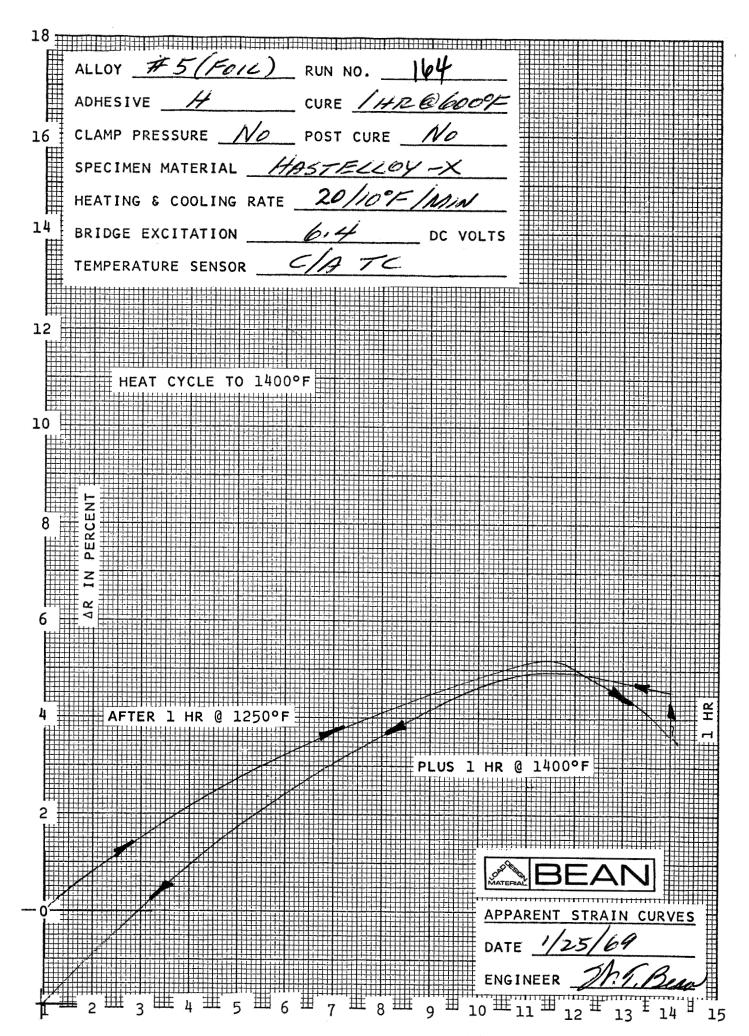


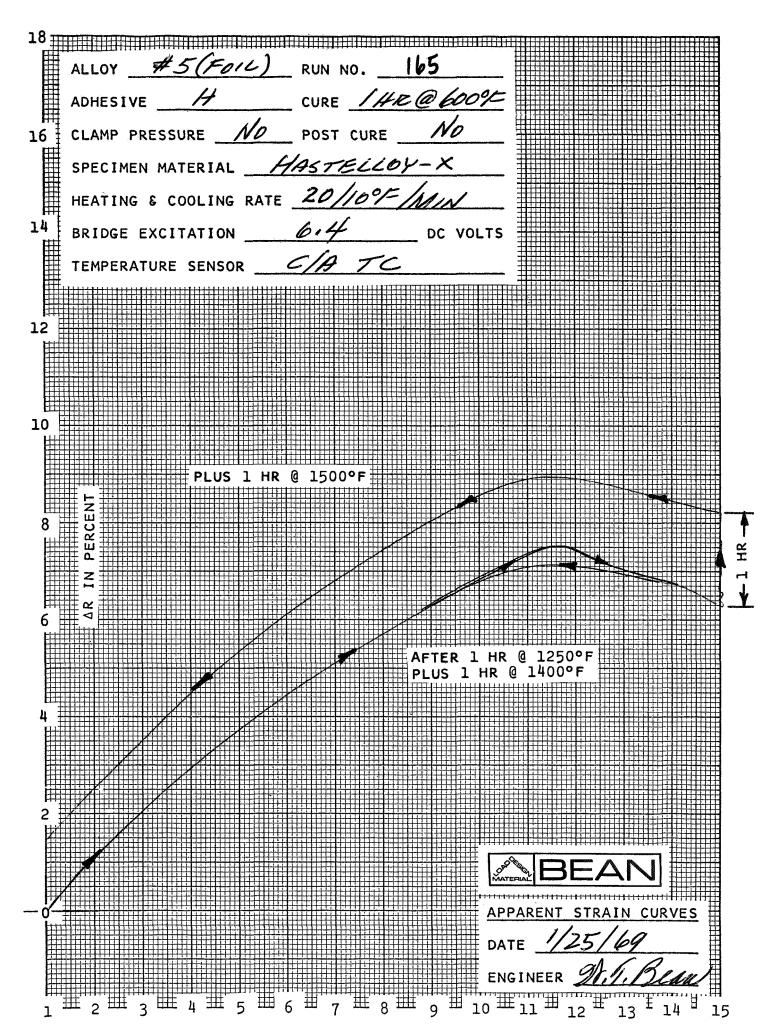


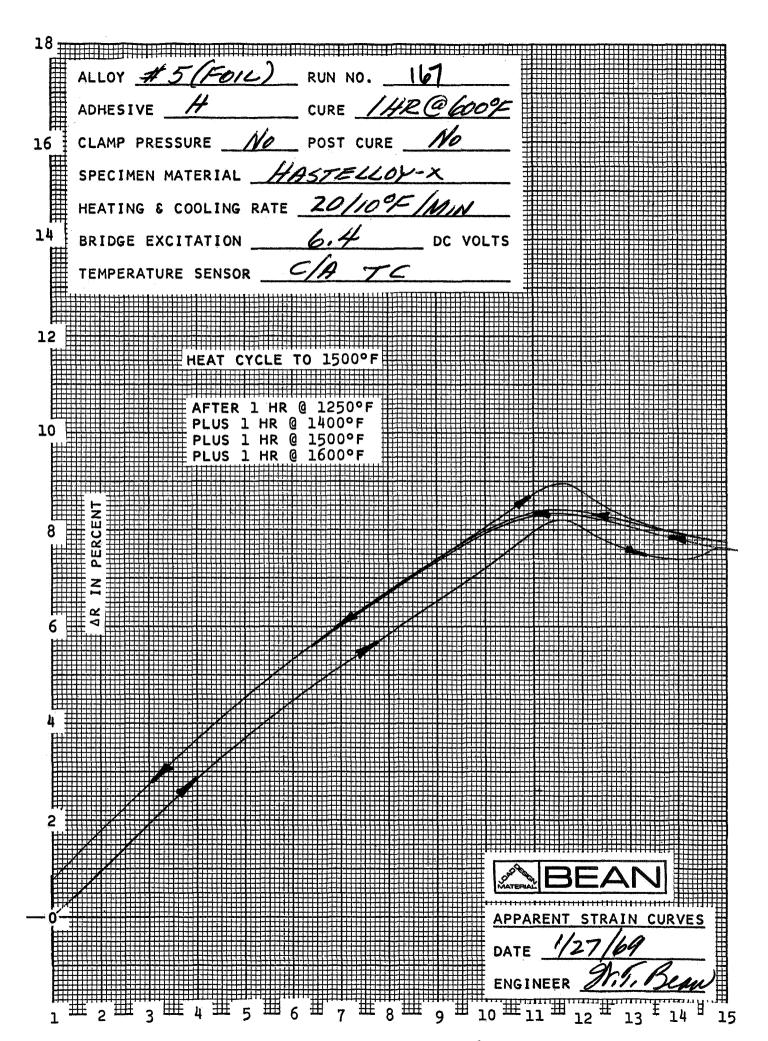


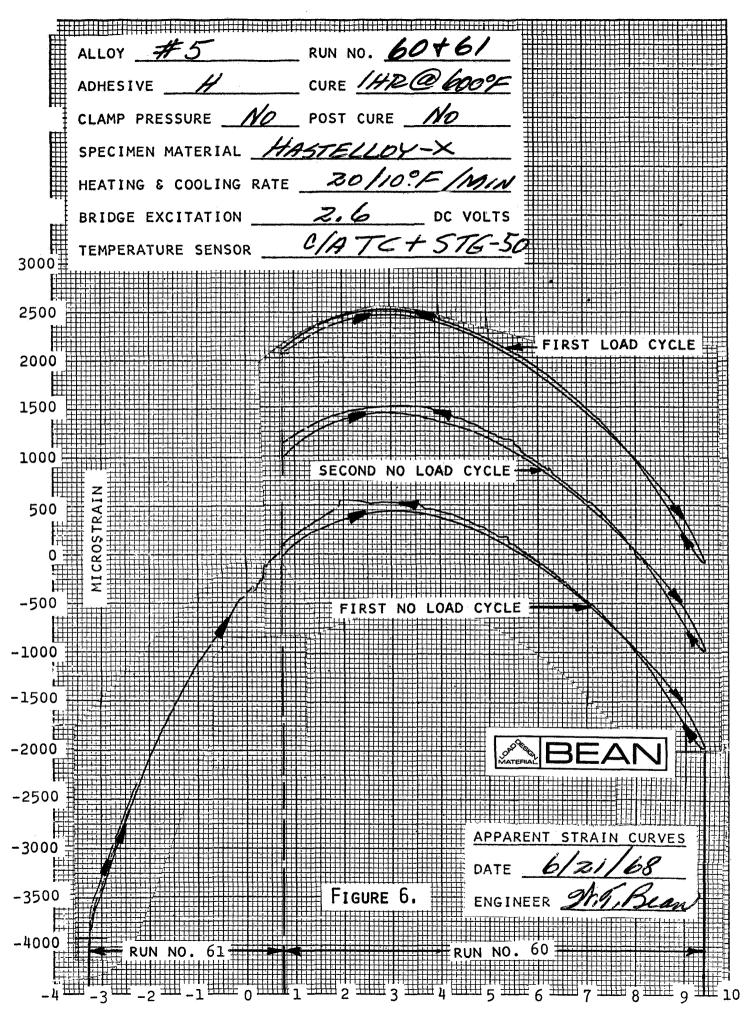
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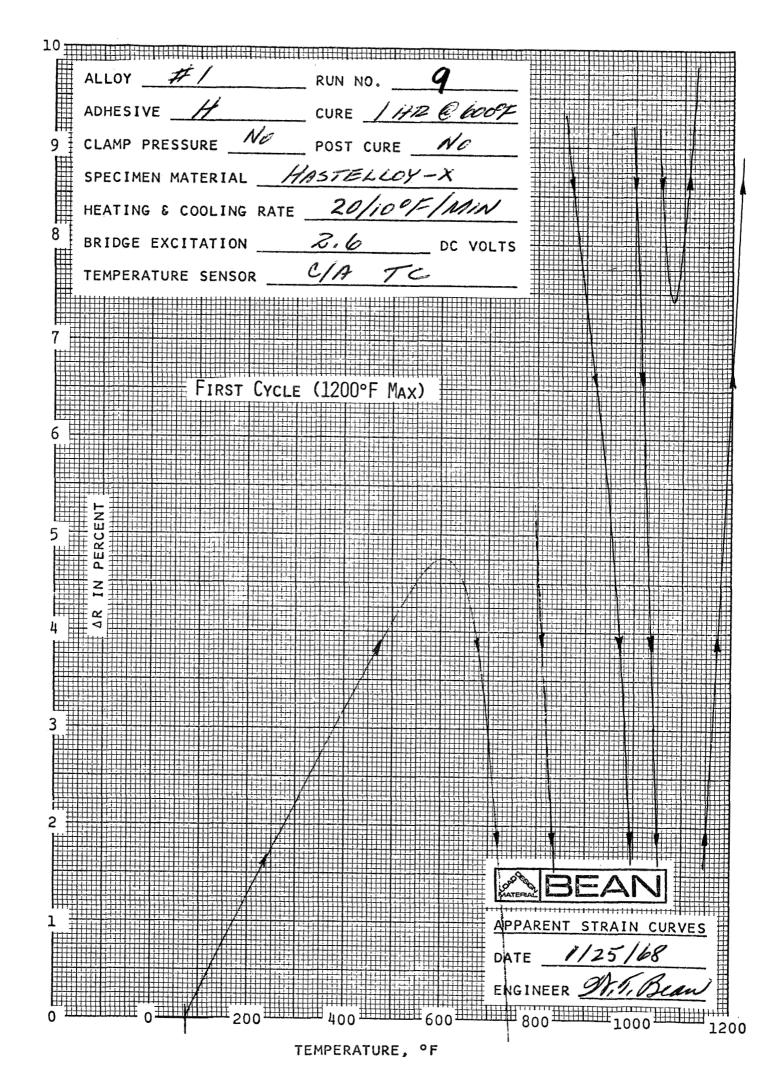




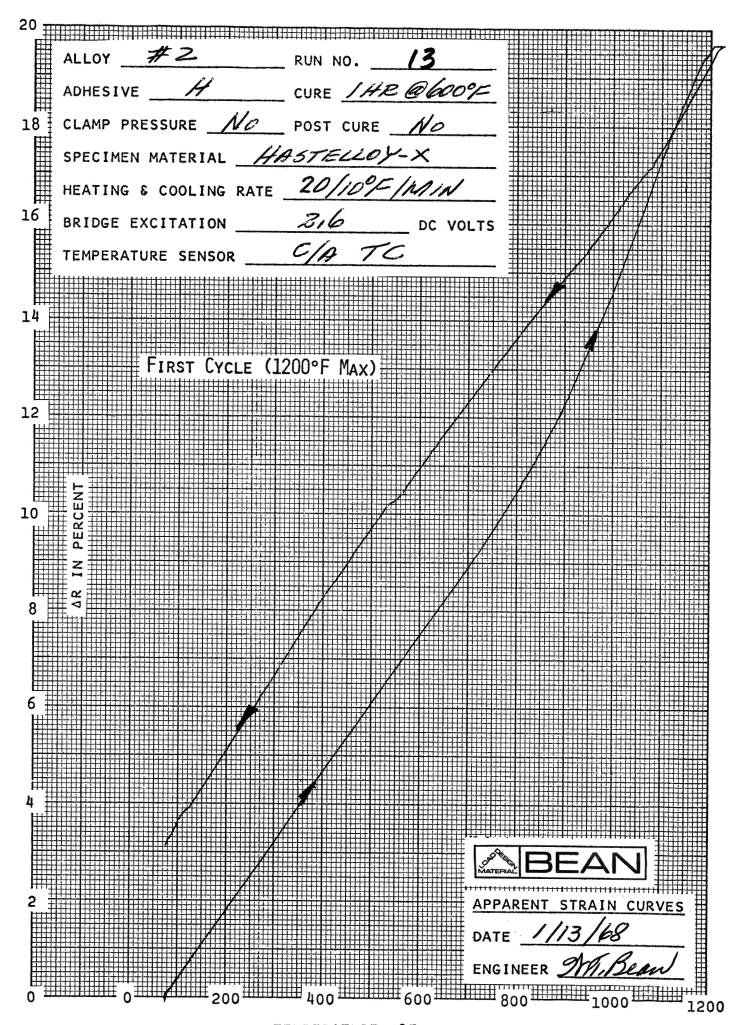


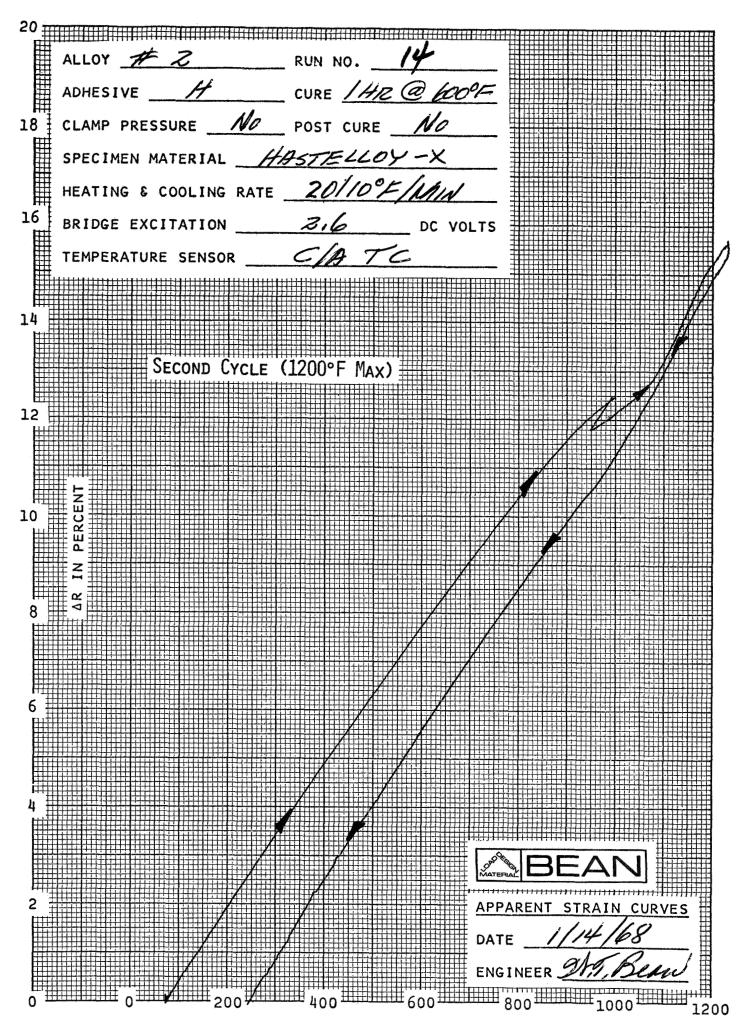


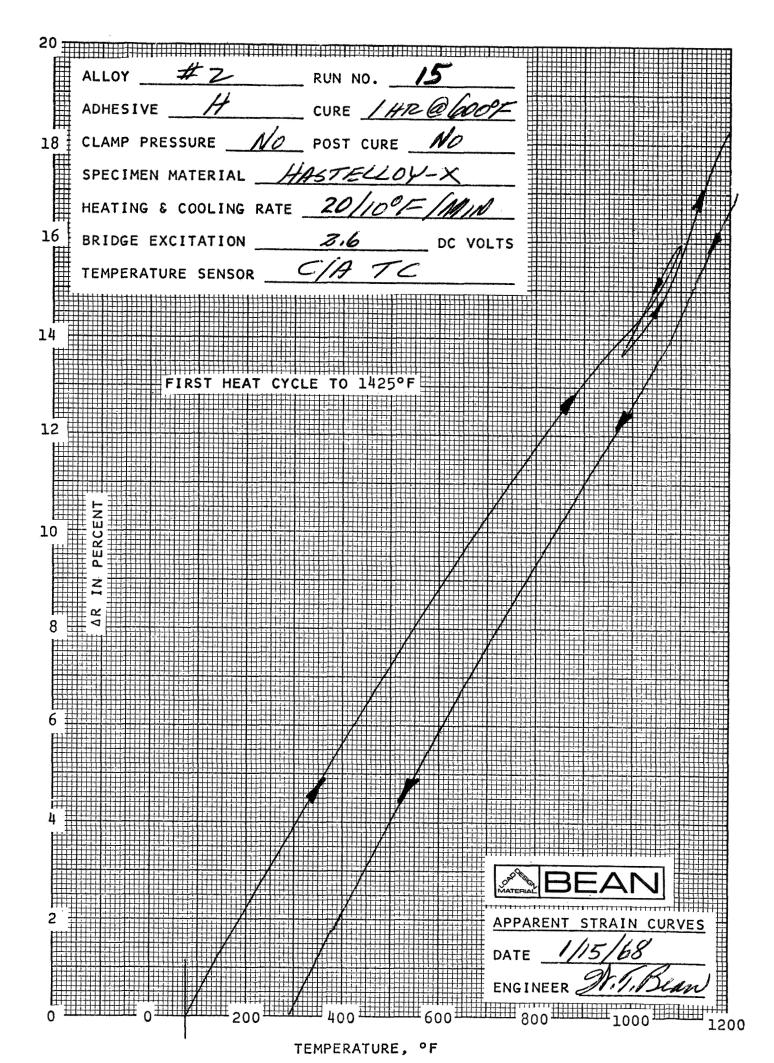


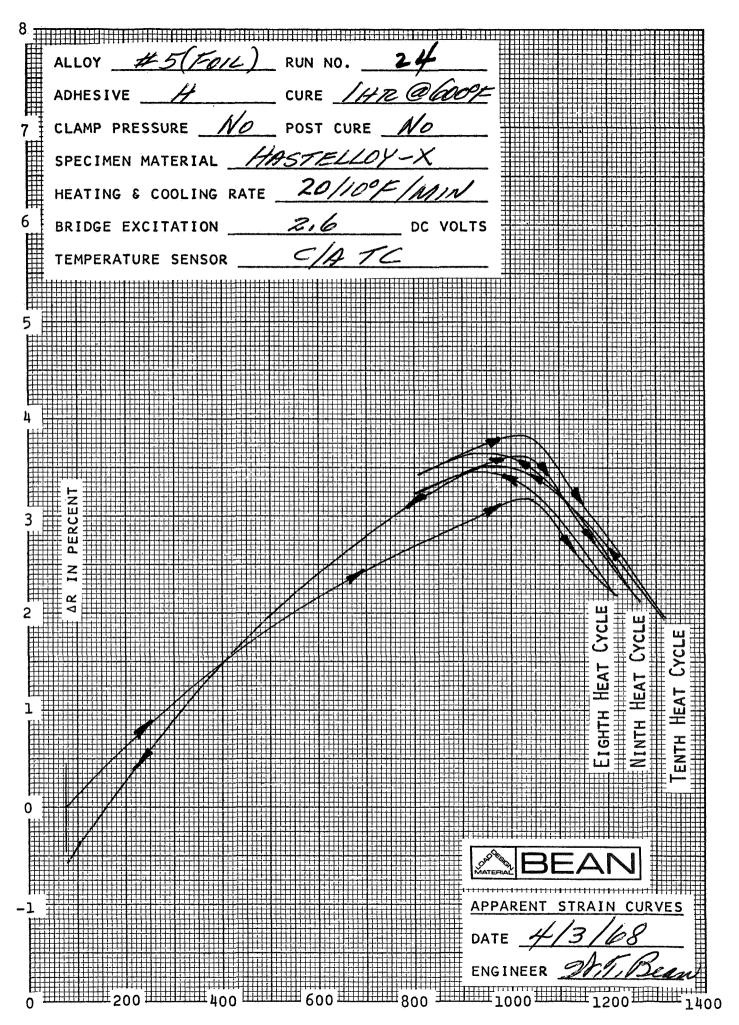


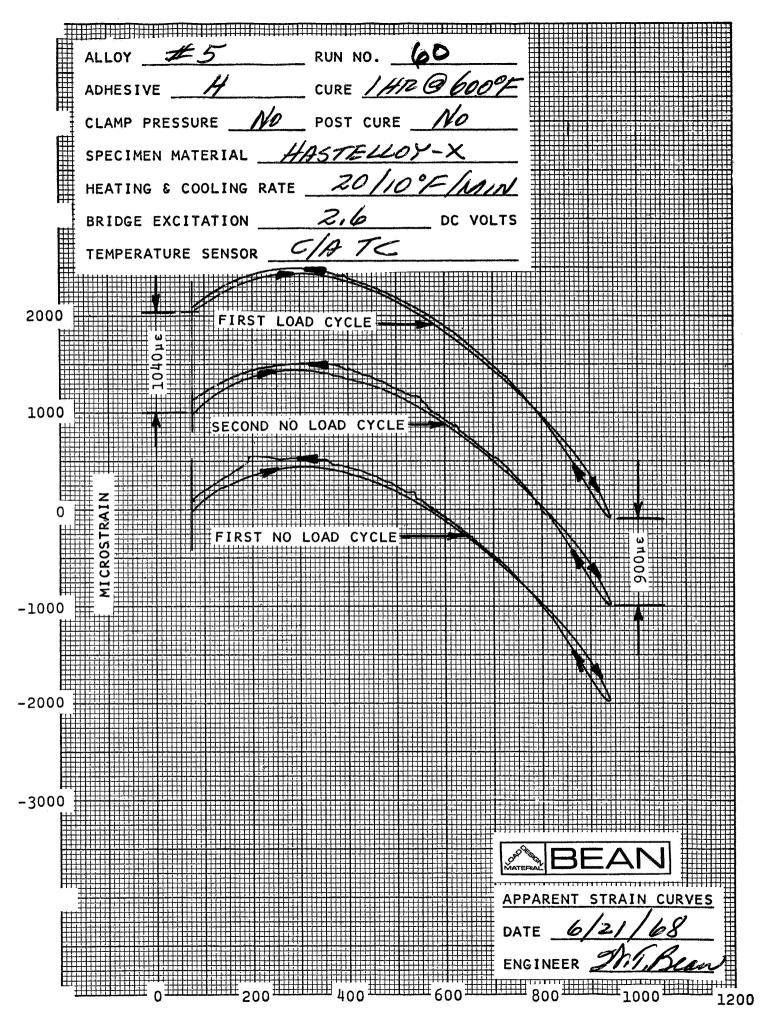
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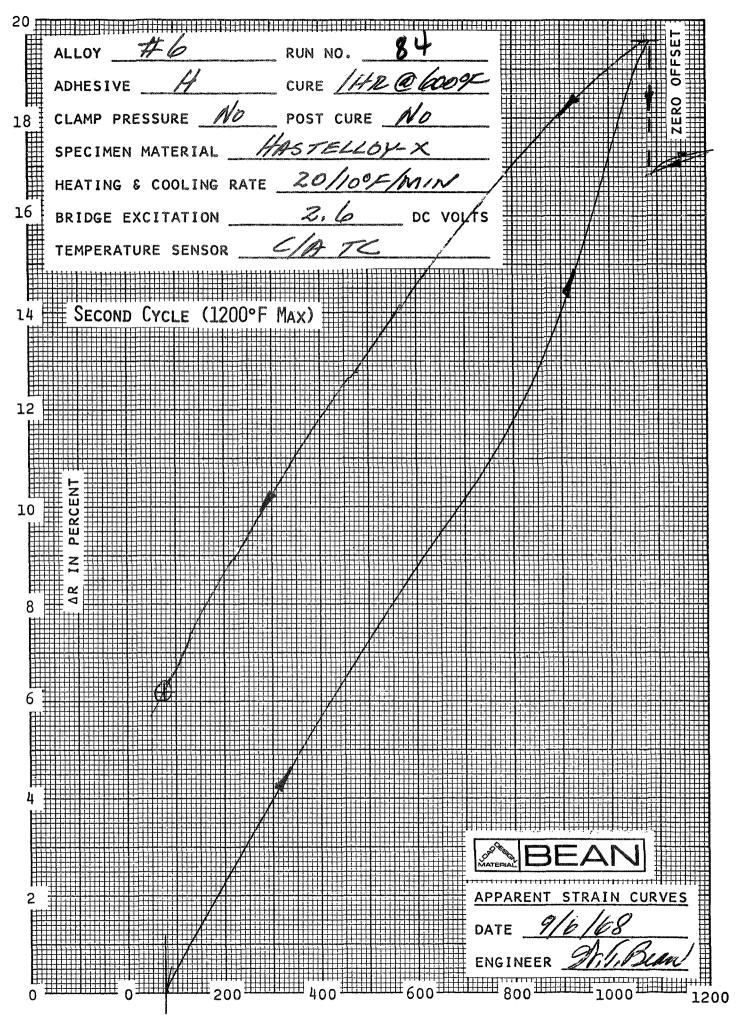


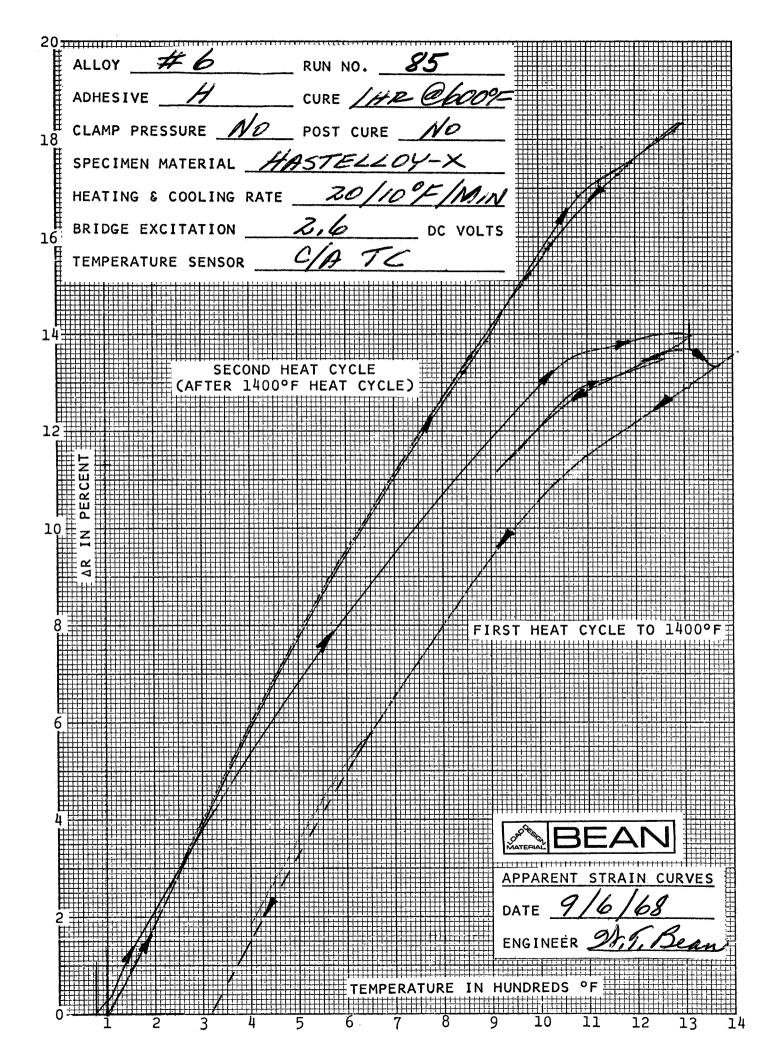


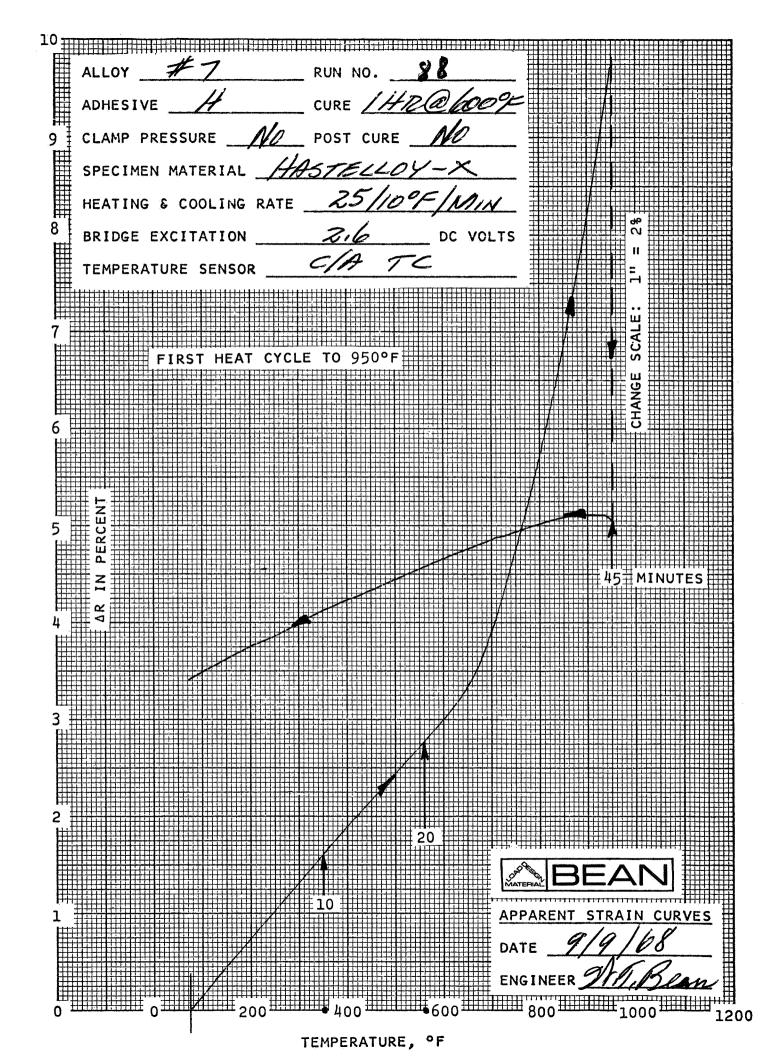


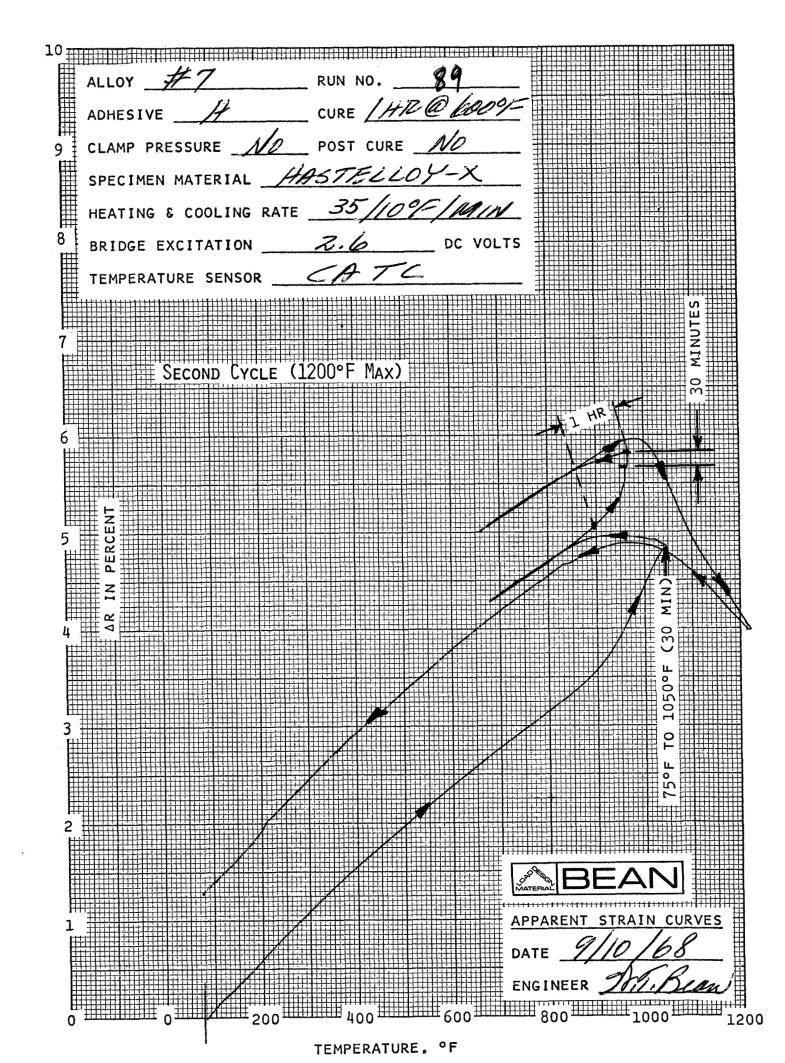


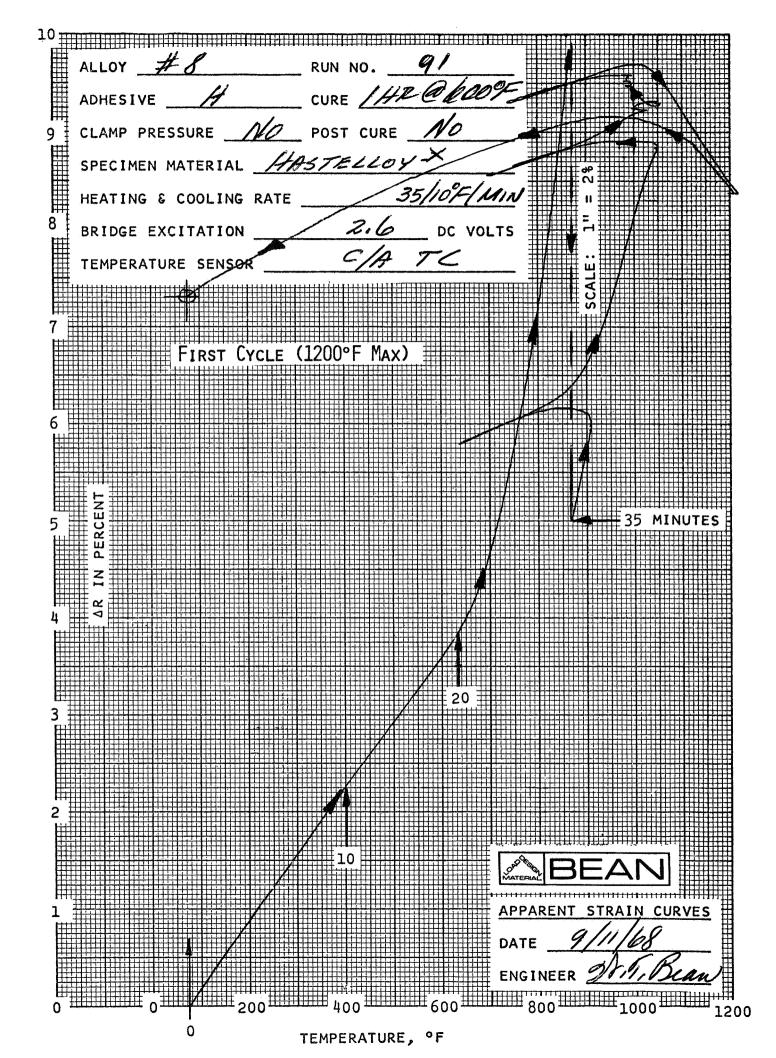


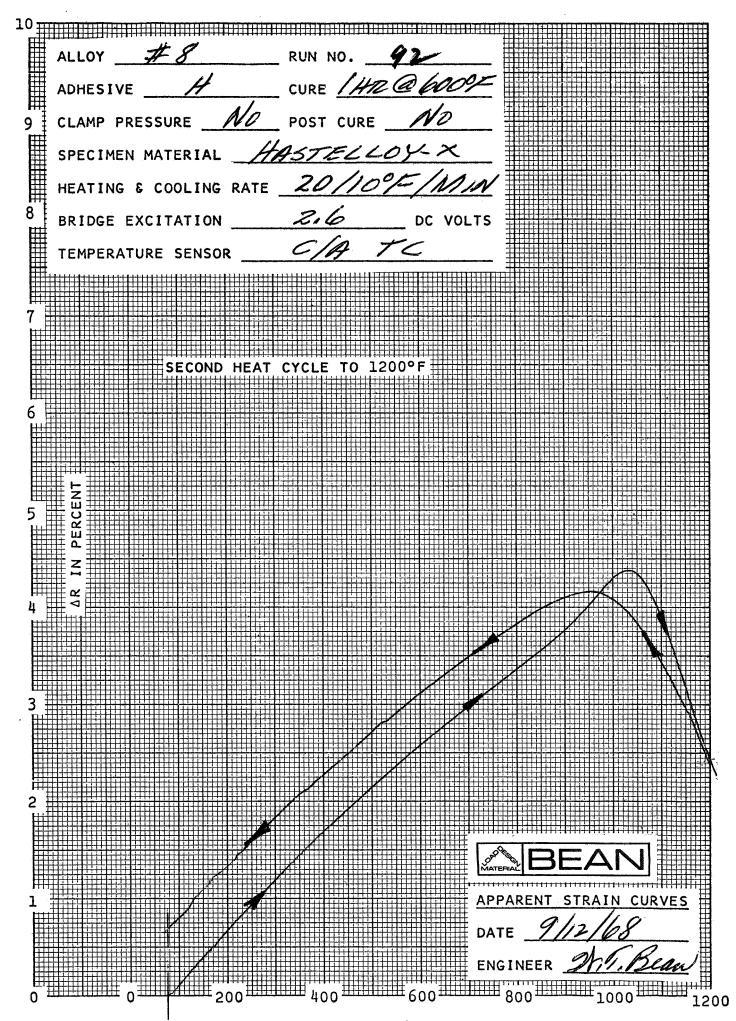




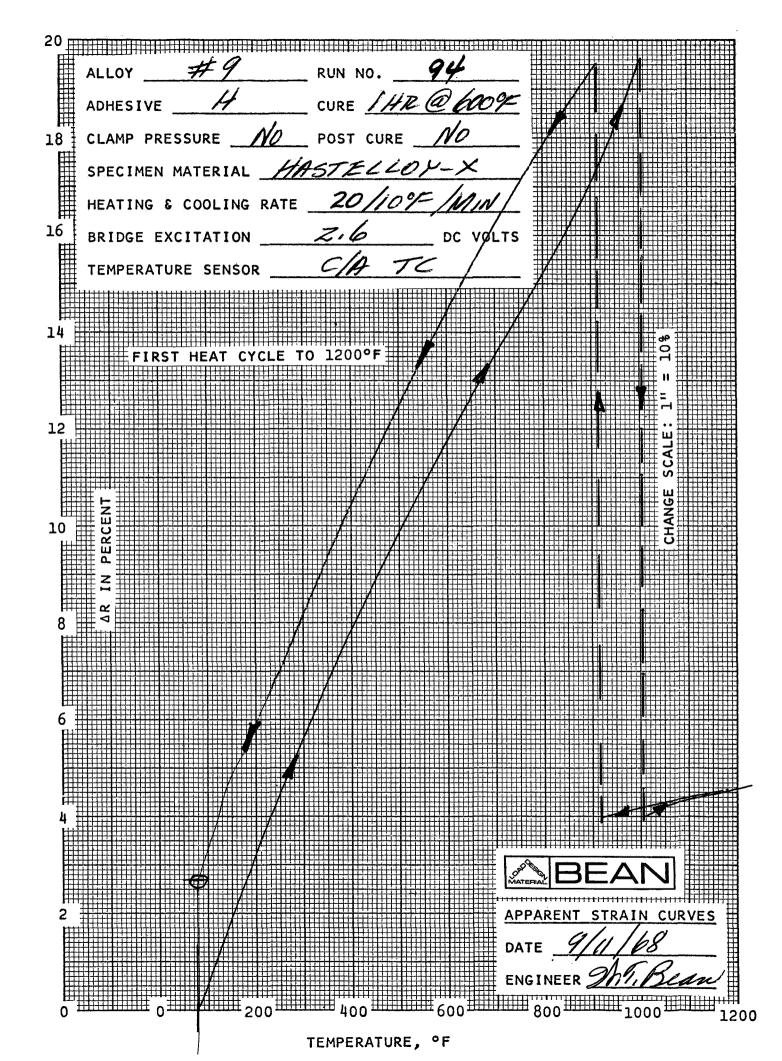


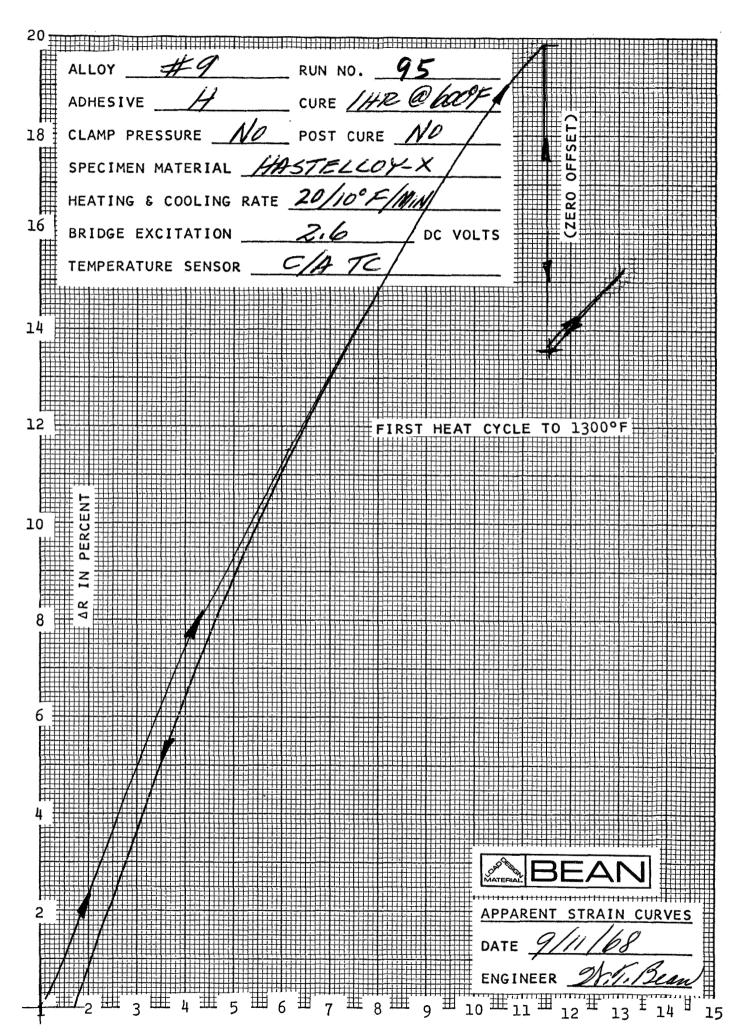




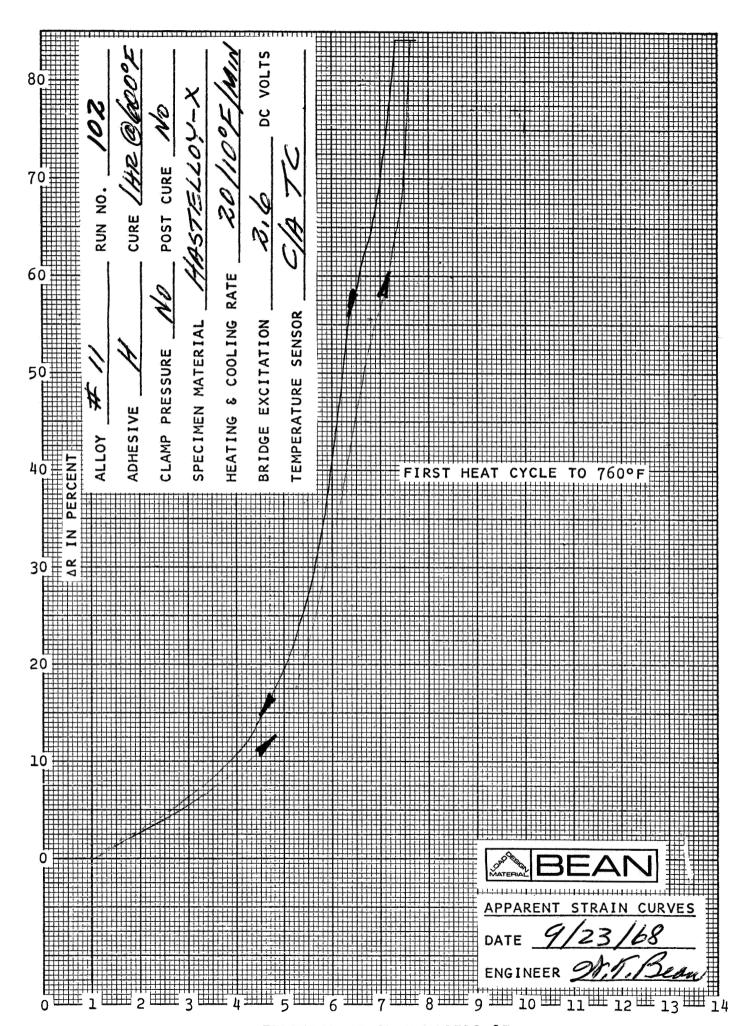


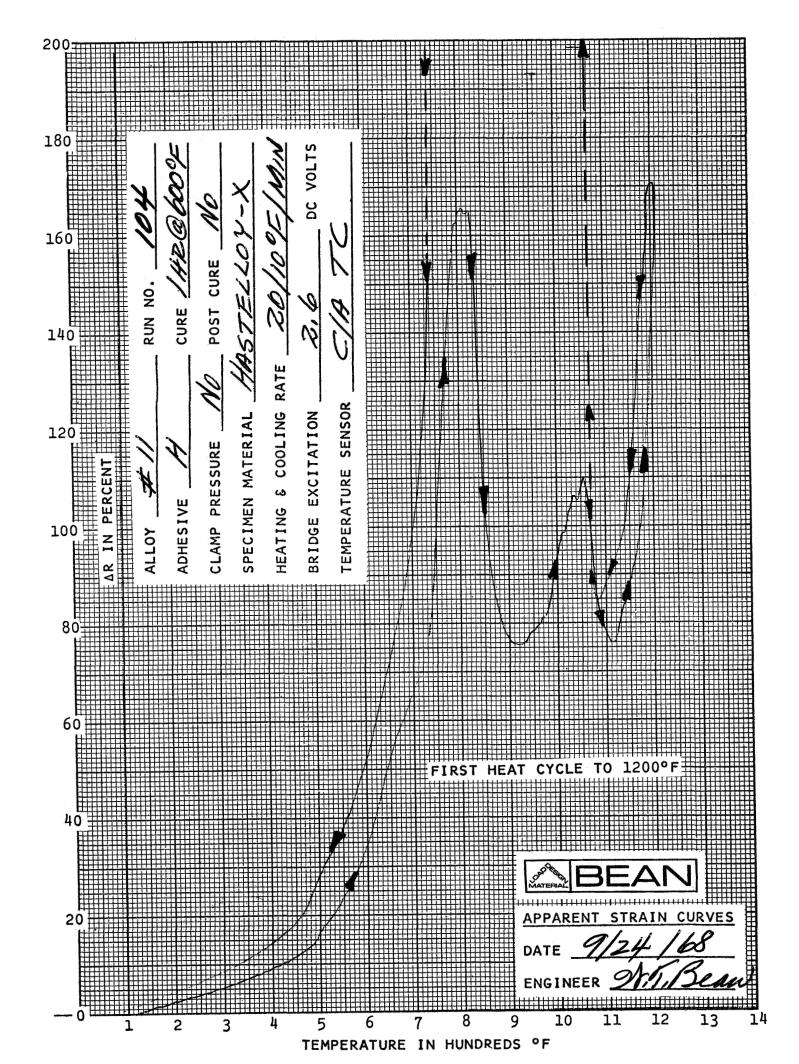
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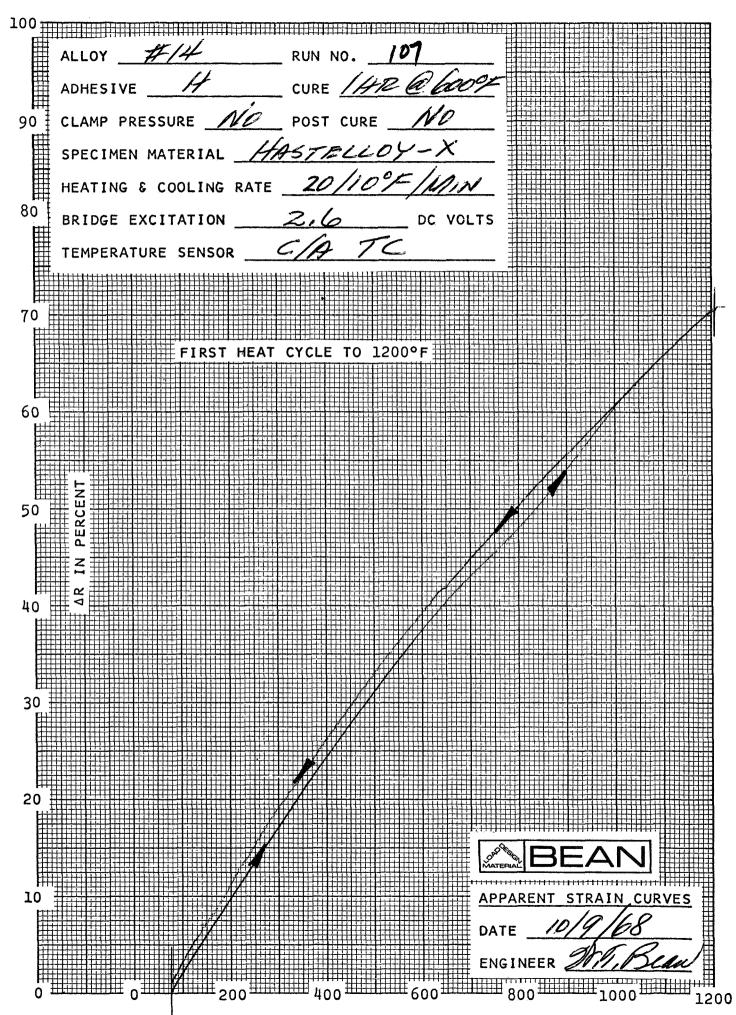




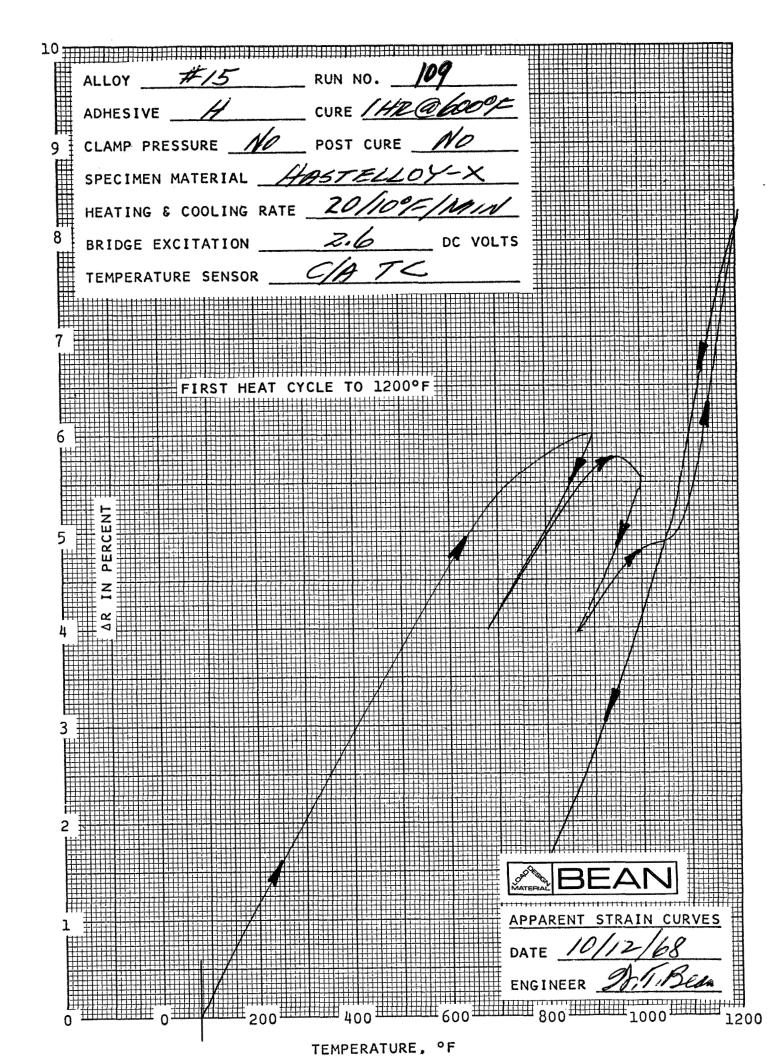
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		RUN NO. 97	
		CURE 142 @ 600%	
	CLAMP PRESSURE NO	POST CURE NO	
	SPECIMEN MATERIAL HAS		
	HEATING & COOLING RATE _		
	BRIDGE EXCITATION	2.6 DC VOLTS	
	TEMPERATURE SENSOR		
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10 4	SECOND HEAT CY	CLE 10 1300°F	
0			
-10	FIRST HEAT CYCLE TO (POLARITY REVERSE	1300°F	
1	2 3 4 5 6	7 8 10 10	12 13







TEMPERATURE, °F



V. STRAIN GAGE DESIGN

A strain gage grid was designed utilizing platinum Alloys # 13 and # 3 (Figure 7). The grid was cemented to a high-temperature test specimen of Hastelloy-X. Figure 8 shows the various apparent strain curves obtained by stabilization at 1300°F.

Tests also were conducted with various lengths of the compensating filament, Alloy # 3, in order to rotate the temperature coefficient (T-C) curve (Runs # 202, # 203, and # 209). These runs are compared in Figure 9.

Temperature compensated strain gages were designed and tested on the materials listed in Table VIII. The gage may be designed for other materials by using Figures 10 and 11.

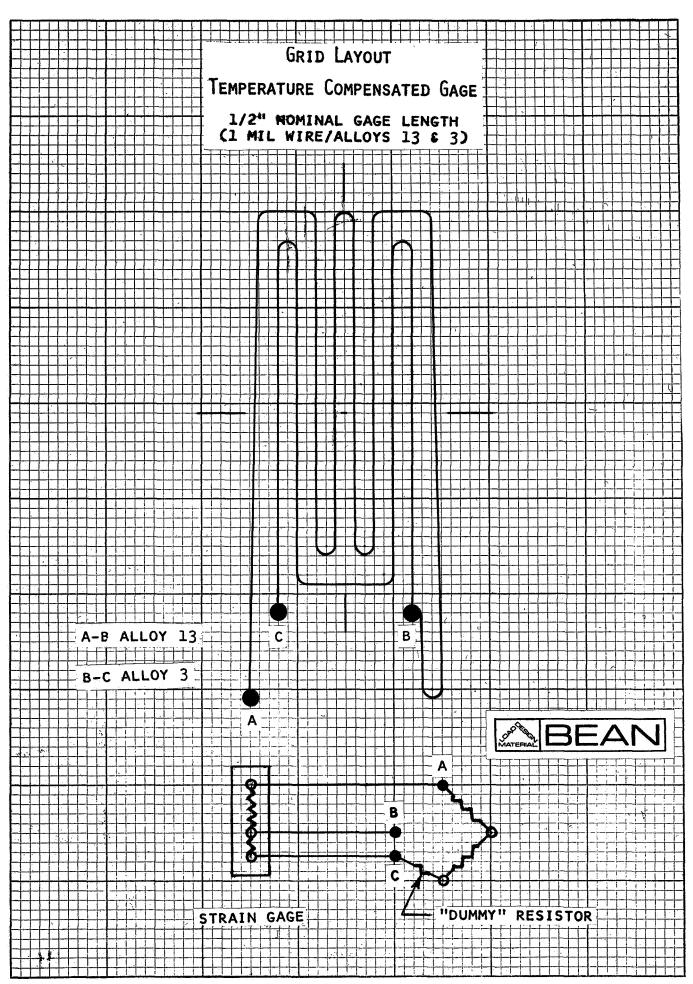
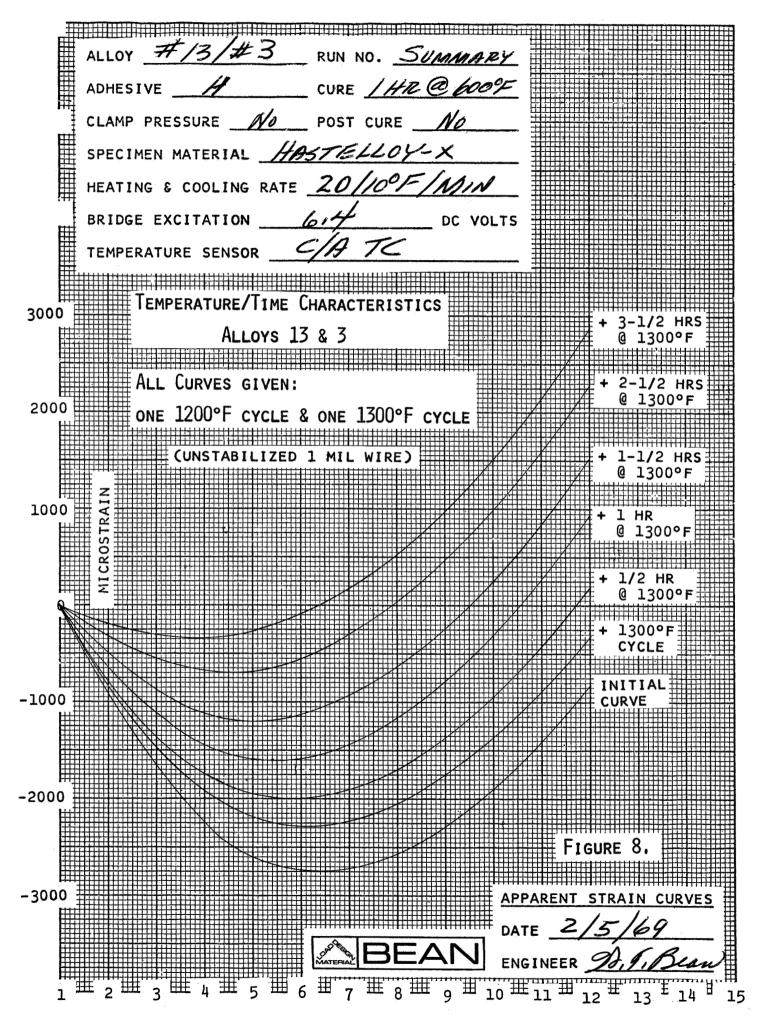
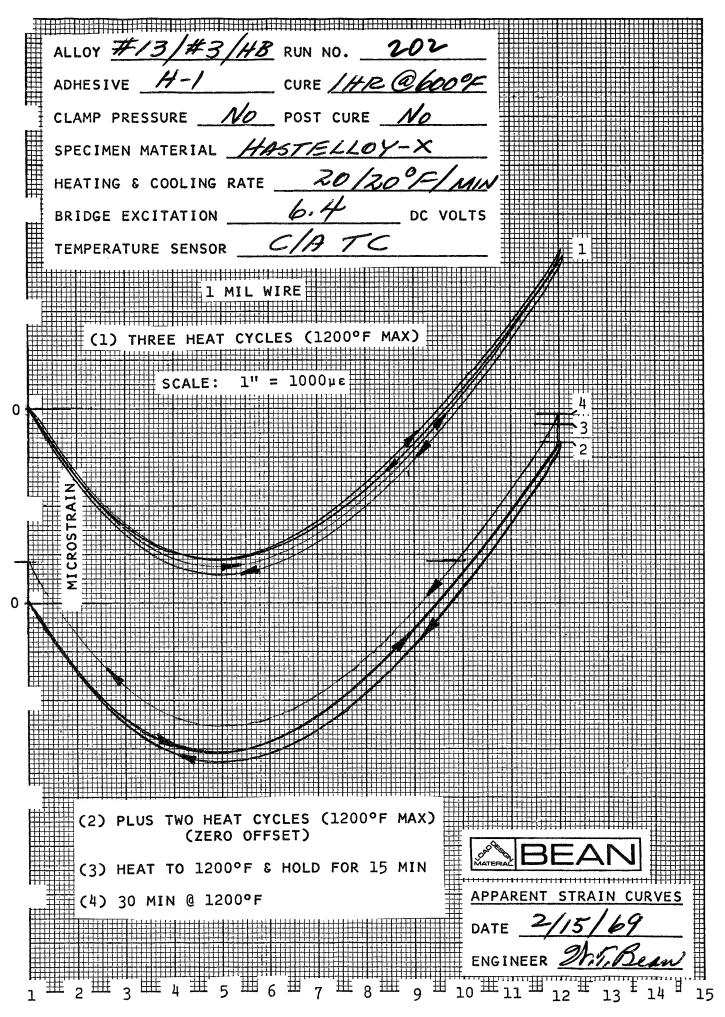
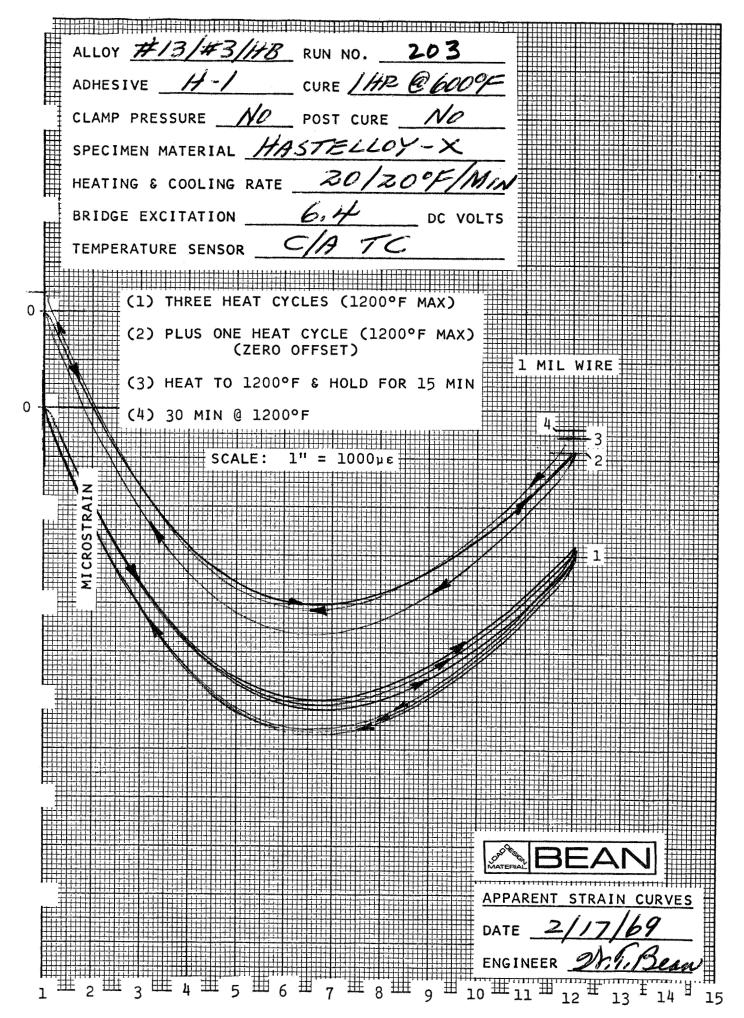
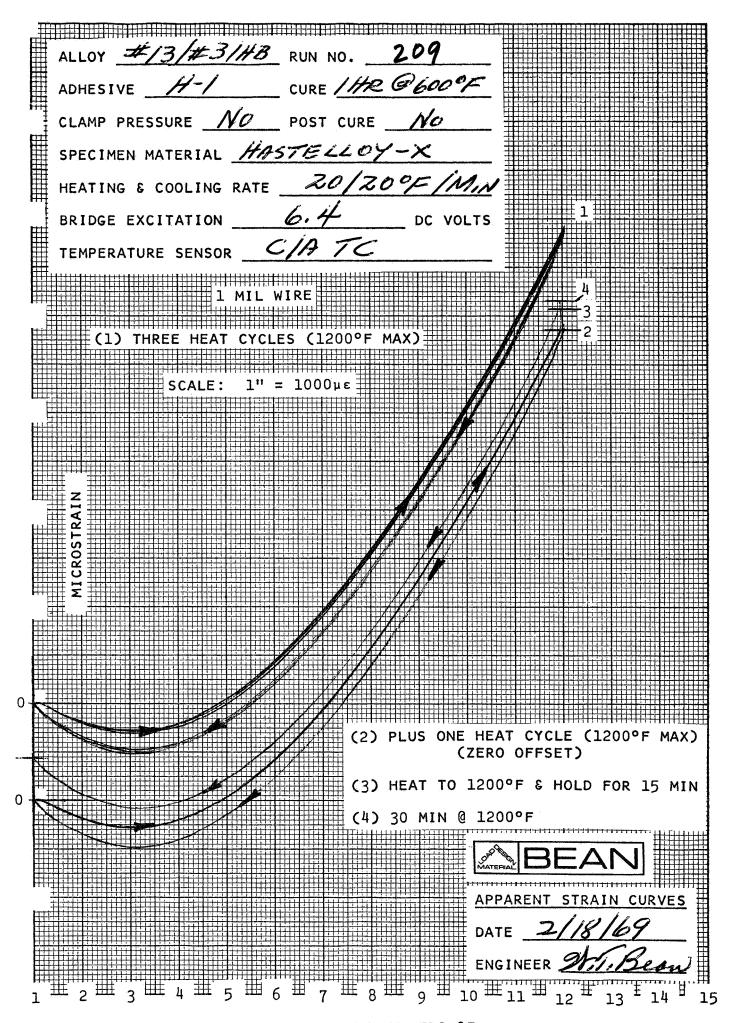


FIGURE 7.









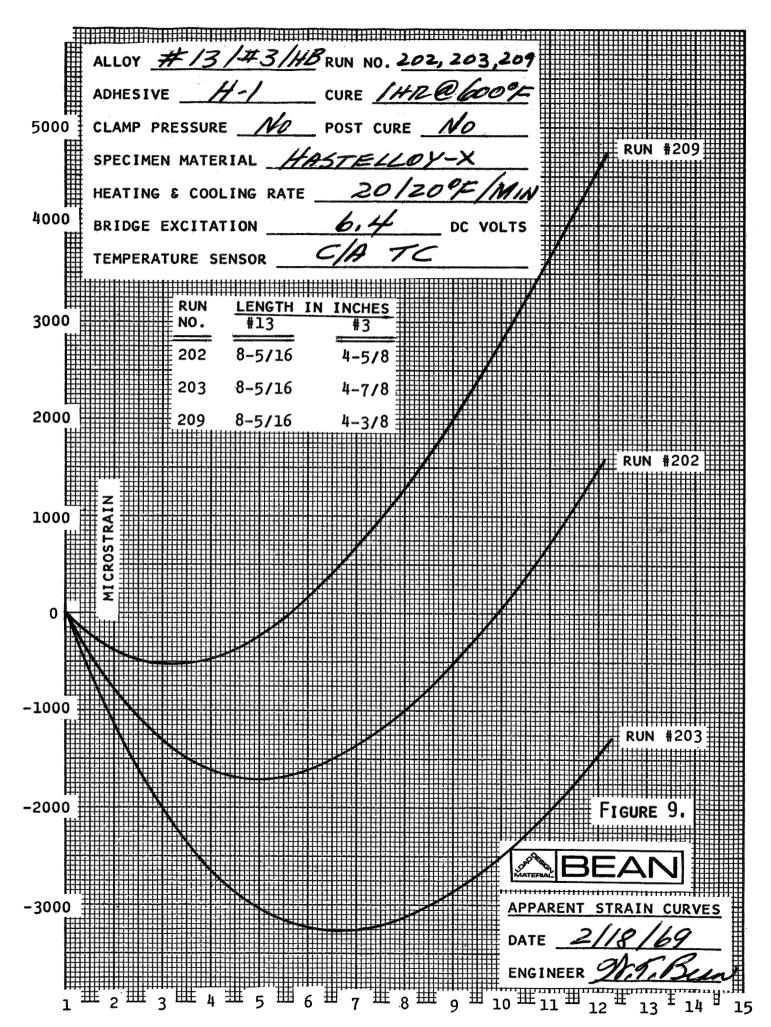


Table VIII

STRAIN GAGE ALLOYS 13 & 3

Typical Compensating Elements for 120 Ohm Gages*

(Based on 1 Mil Wire)

Specimen Material	Expansion Coefficient PPM/°F	Length in Inches	Compensating Resistance Ohms	"Dummy" Resistance Ohms
Zirconium	3.1	2-3/32	34.95	85.05
Titanium	4.9	2-3/16	36.51	83.49
17-4 PH	6.0	2-7/32	37.03	82.97
Hastelloy-X	7.7	2-11/32	39.12	80.88
304 SS	9.3	2-13/32	40.16	79.84

*Nominal length of 120 Ω active element (#13) is 4-3/16" @ 75°F



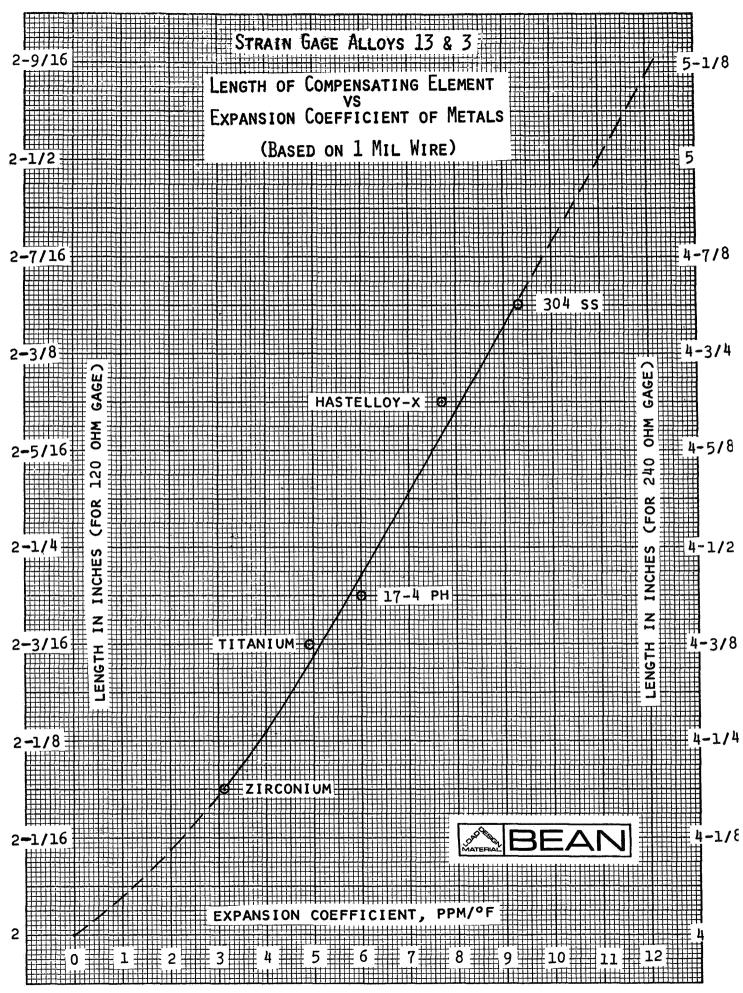


FIGURE 10.

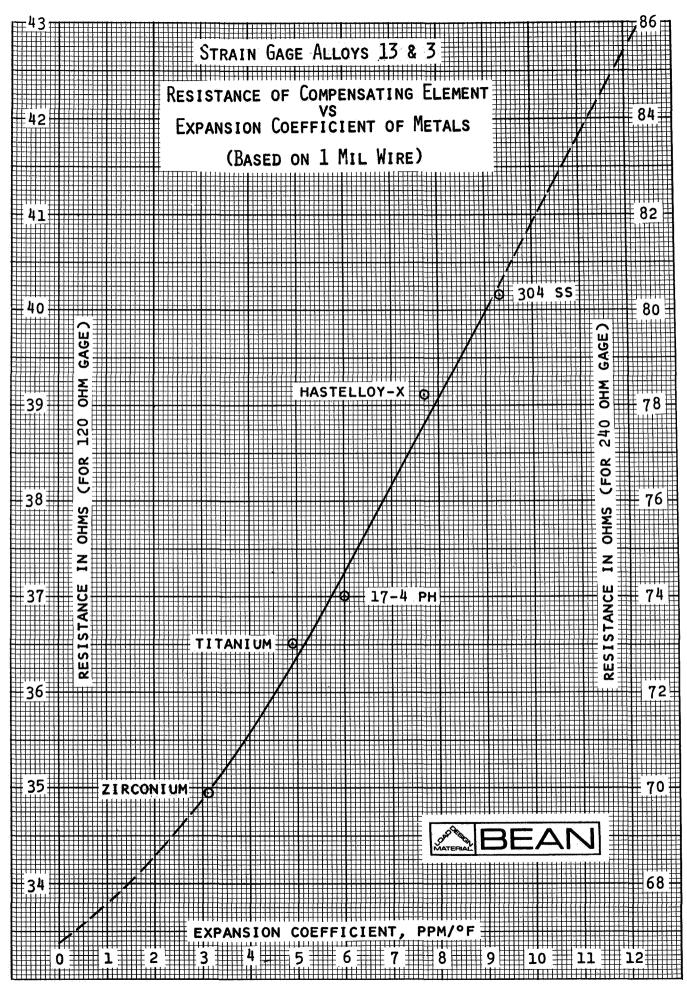


FIGURE 11.

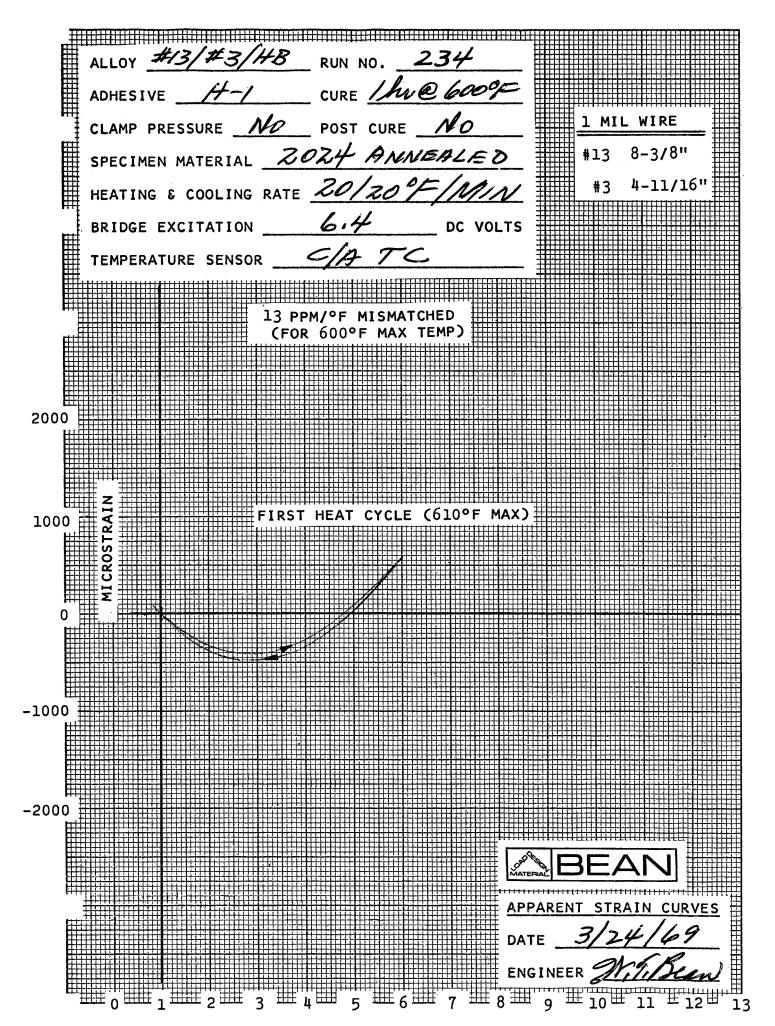
VI. STRAIN GAGE EVALUATION

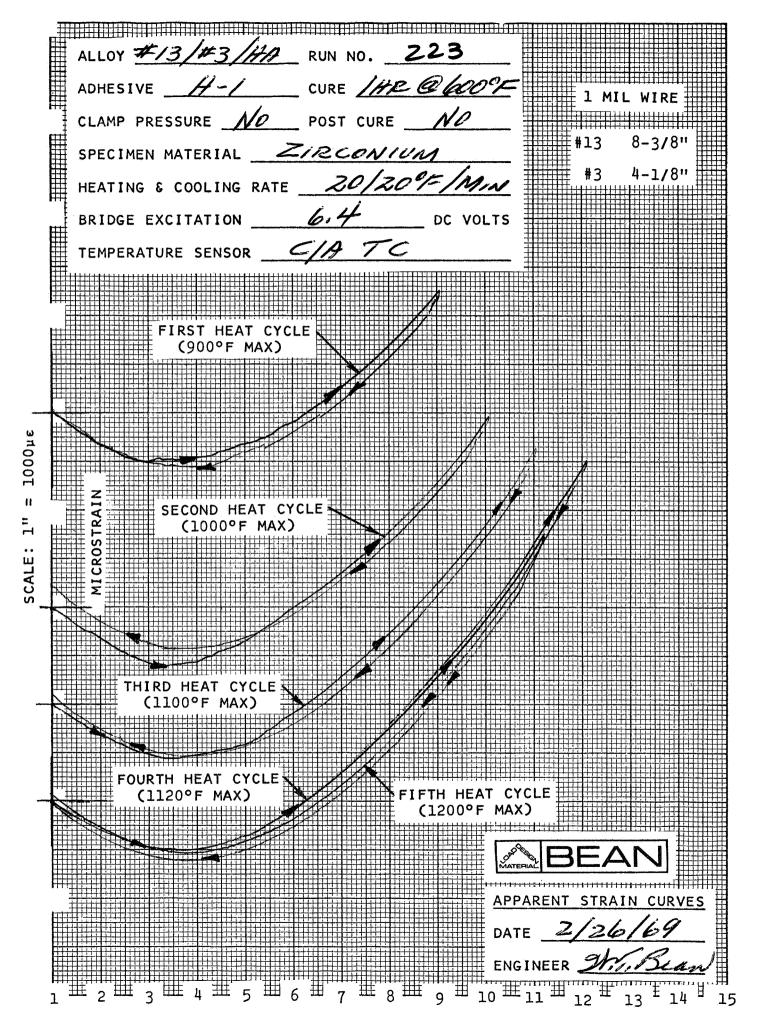
Temperature Compensation

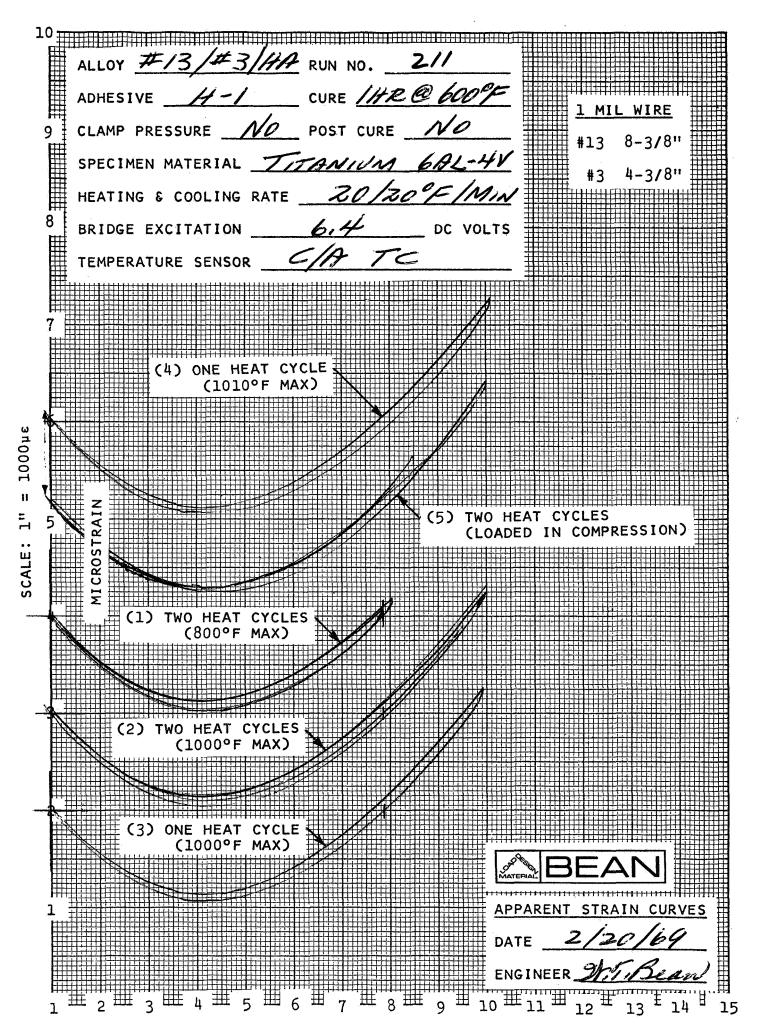
Using the preceding information, apparent strain curves were obtained as follows:

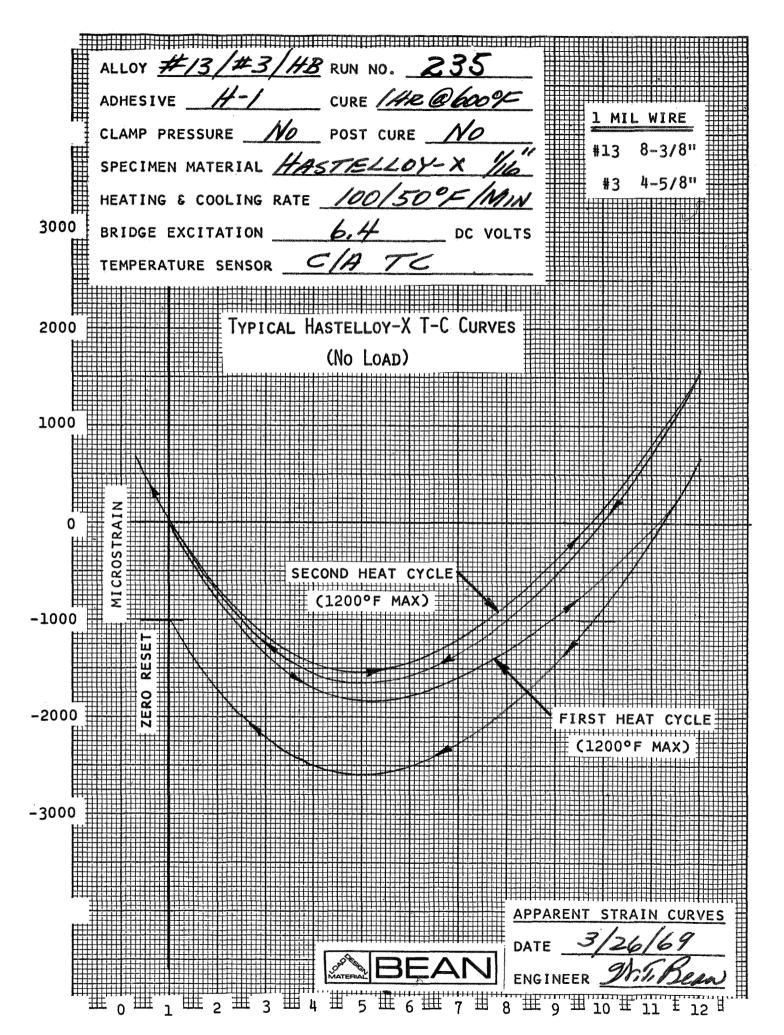
Specimen Material	Run No
Aluminum, 2024	234
Zirconium	223
Titanium, 6AL4V	211
Hastelloy-X	235
Hastelloy-X	230
Stainless Steel, 304	214

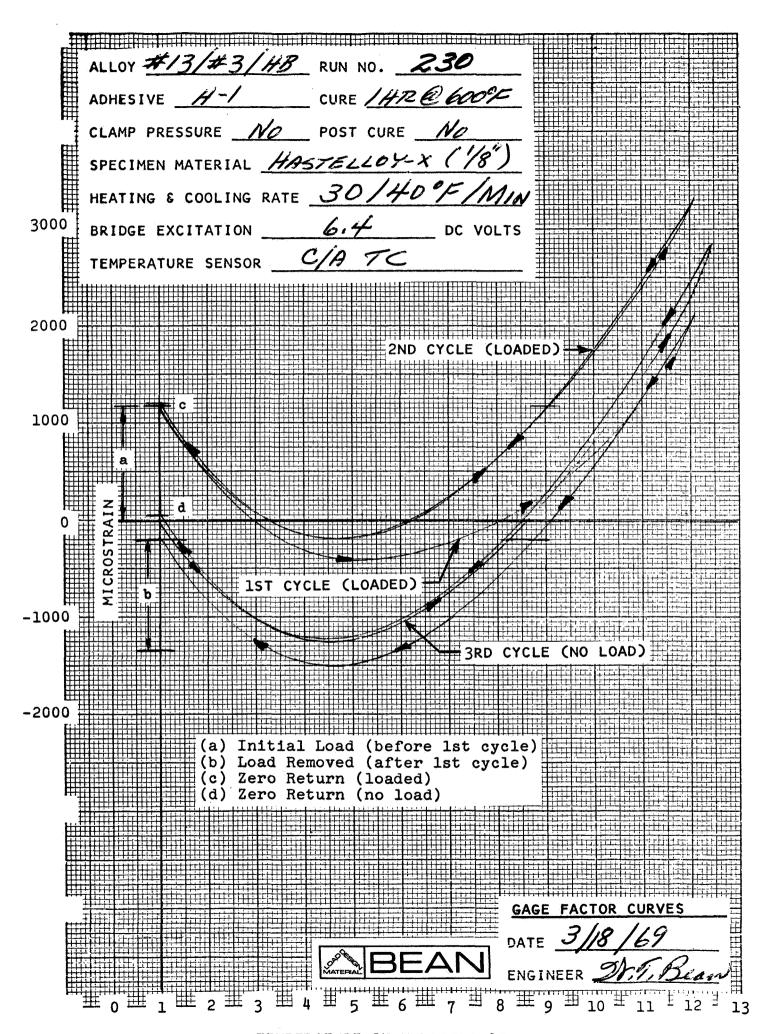
During the initial heat cycle a zero offset is evident when the strain gage filament encounters plastic deformation (Runs # 235, # 230, # 214). The magnitude of the offset may be predicted by considering the coefficient of expansion of the specimen material and the applied mechanical strain. The gage filament performs in an elastic manner on the recovery cycle.

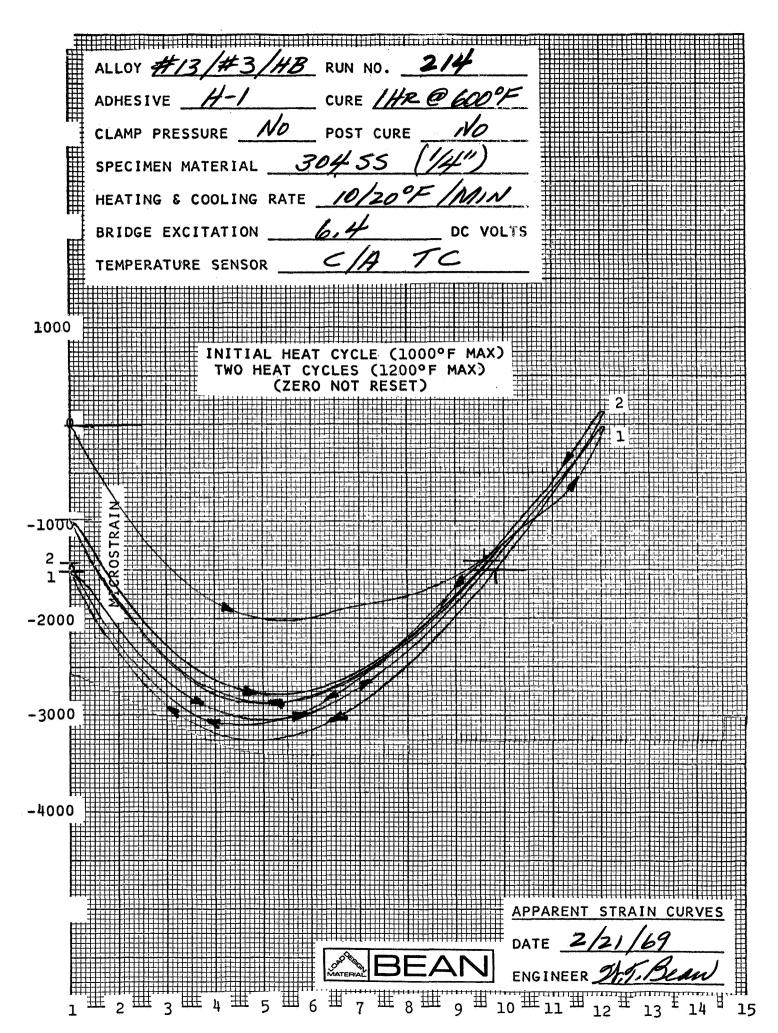












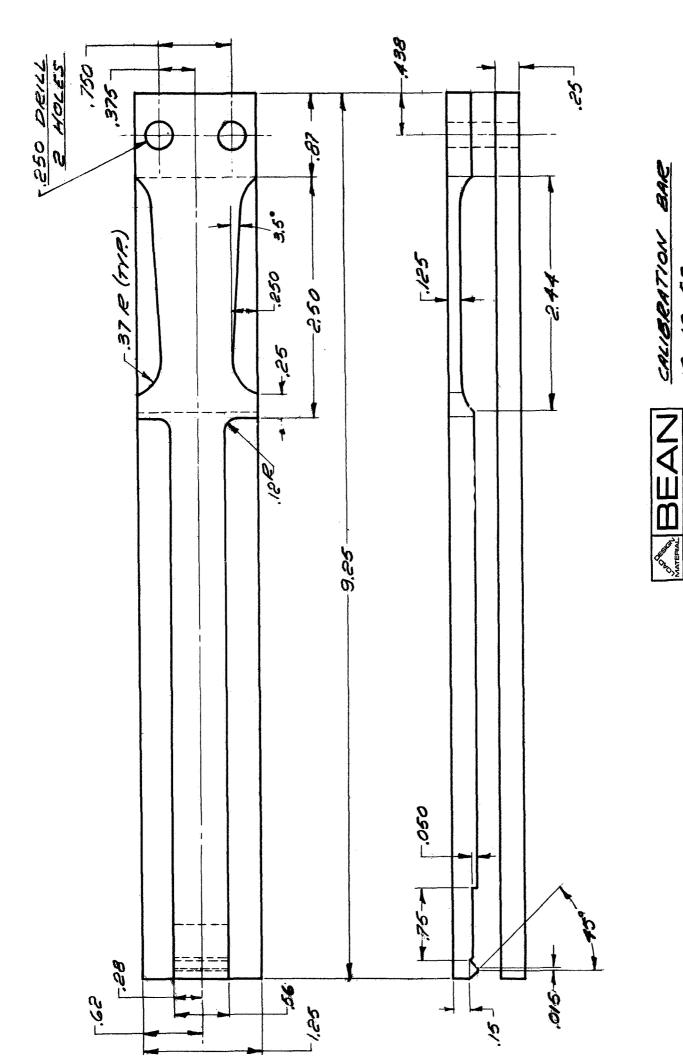
Gage Factor vs. Temperature

In order to determine gage factor vs. temperature, a strain gage was mounted on the gage-factor calibration bar (Figure 12). "First" cycle point-by-point data was obtained at various temperatures (Table IX). The second cycle T-C curve is shown (Run # 200). The third heat cycle (no load) is compared with the fourth heat cycle (fixture loaded) (Run # 201). The reduction in gage factor with increasing temperature is apparent from closer ordinate spacing at higher temperatures.

Table X is a record of a test conducted by mounting a similar gage on a second calibration bar. A Time/Temperature Chart of the test is shown (Figure 13). Run # 221 charts the initial (no load) heat cycle. Approximately eight hours of testing followed (Run # 222).

Run # 219 indicates the zero offset obtained from a strain gage with an alternate heat treatment. Tables XI and XII list the test record of a strain gage mounted on a similar fixture. The fixture was fabricated from J1650, a "Superalloy" used for gas turbine blades. The Time/Temperature Chart is shown in Figure 14. Approximately twenty hours of test results are graphically presented in Runs # 224, # 225, # 226. Results of numerous gage factor vs. temperature tests were plotted (Figure 15).

Two gages were mounted in a back-to-back (bending) configuration on the test specimen (Figure 4). The T-C curves of each gage were compared (Runs # 144, # 145). Load and no load runs were conducted, using different pin diameters in the fixture. Run # 146 was conducted using 1/4" pins, while Run # 147 was conducted with 3/16" pins. The results are in agreement with data from Figure 15.



W. T. BEAN JR. 1.1.1. CALIBRATION 12-18-57 DESIGNED ORAWN

Figure 12,

SCALE: FULL SIZE

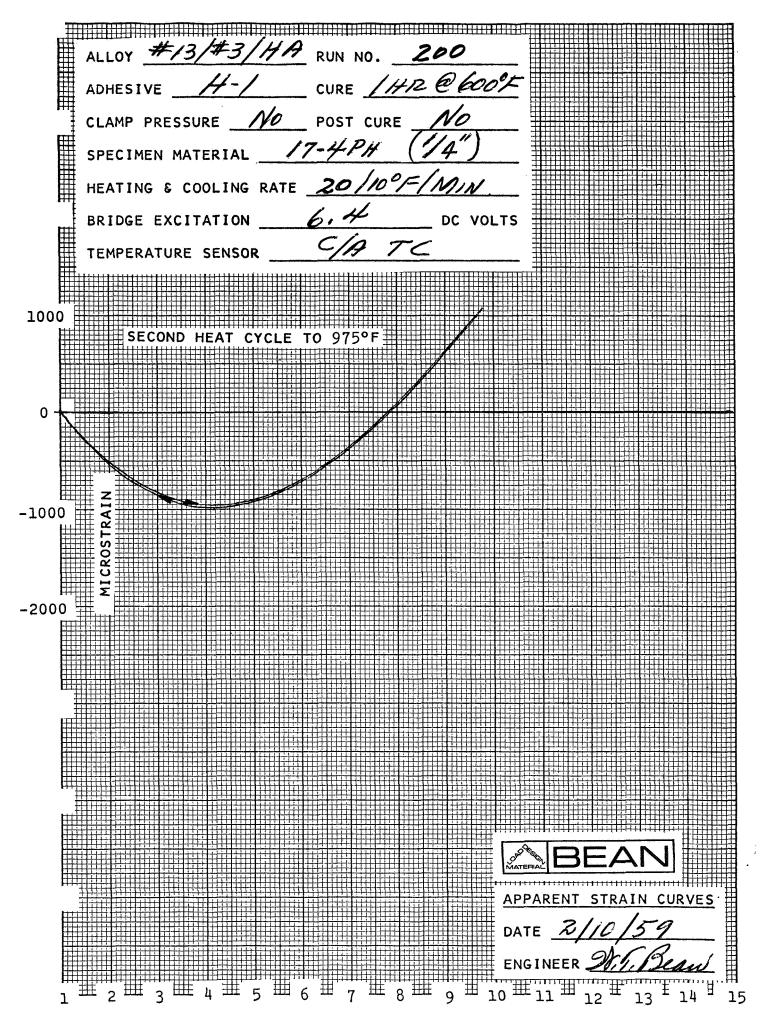
Table IX

<u>Gage Factor vs Temperature</u>

First Cycle Point by Point Data*
(Prior to Runs #200 & #201)

Test Temperature	Apparent Strain	Load Strain	Percent G.F./100°F
100°F	0 με	586 με	100.0
250	-711	555	94.7
400	-970	525	89.6
450	-981		interes atomic martin
600	-724	492	84.0
786	0		, MAN - COST - COST
800	42	465	79.4
975	1045	451	77.0
800	46	463	79.0
600	- 758	492	84.0
500	-961	-	non, inc. 444
400	-1012	525	89.6
250	-737	etten etten minn	oper jours com
100	-16	586	100.0

^{*17-4} PH Test Fixture, 1/4" Section Alloy #13/#3



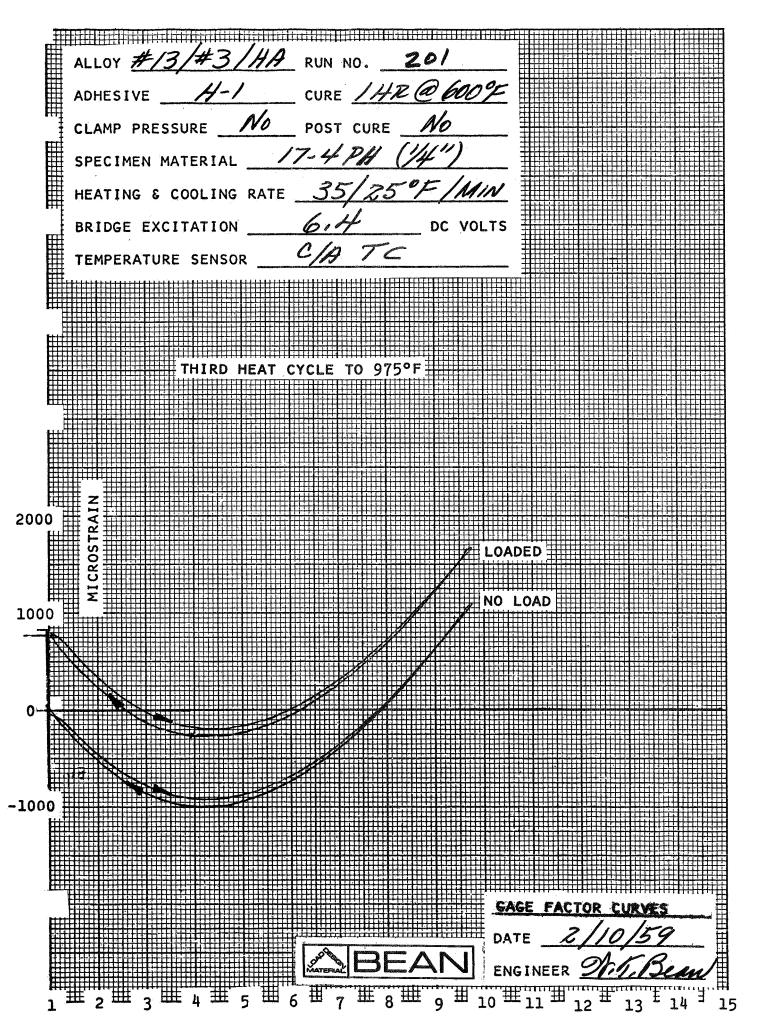


Table X

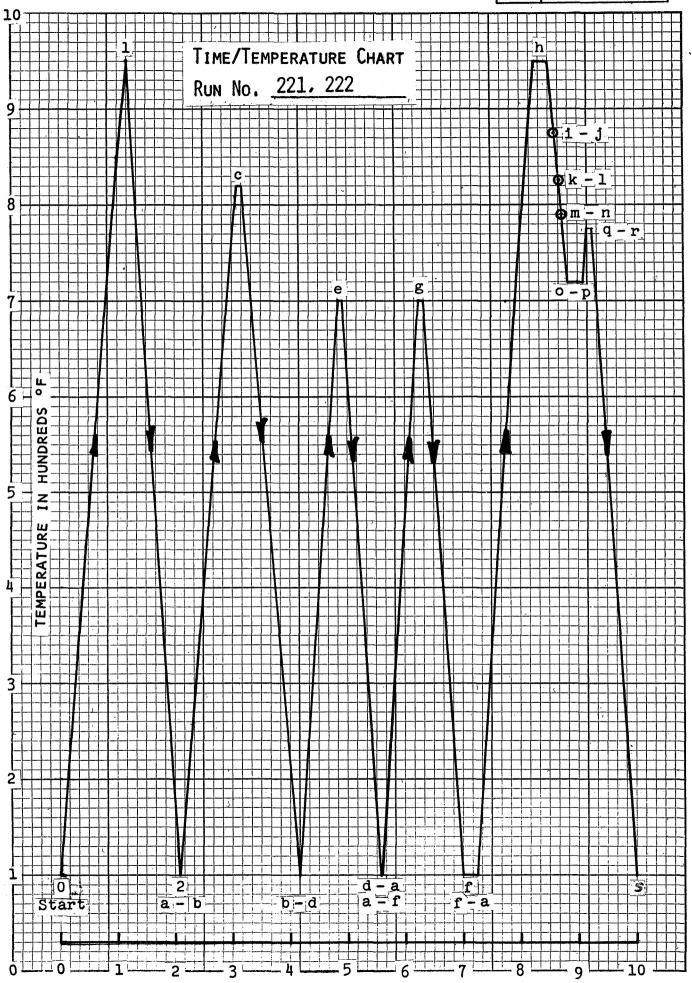
RECORD OF TEST ON 17-4 PH FIXTURE

RUN NO. 221, 222

TEST EVENT	DESCRIPTION OF TEST	LAPSED TIME
0-1 1-2	Heat (100°F to 950°F) no load Cool (950°F to 100°F) in air	1:10 2:05
d-a a-f f-g g-f f-a a-h h-i i-j j-k k-l l-m m-n	Load (+870µε) 100°F Heat (100°F to 820°F) loaded Cool (820°F to 100°F) loaded Load (+1620µε) 100°F Heat (100°F to 700°F) loaded Cool (700°F to 100°F) loaded Unload at 100°F Load (-2100µε) 100°F Heat (100°F to 700°F) loaded Cool (700°F to 100°F) loaded Unload at 100°F, standby Heat (100°F to 950°F) no load Cool (950°F to 875°F) no load	2:06 06 1122 3:1122 4:537 89 55:3150 55:10 77:137 88:340 88:4450 10 88:510 88:510
q-r	Unload at 775°F Cool (775°F to 100°F) no load Zero Offset (-30µc) in 7:55 hrs	9:11 10:00 hrs

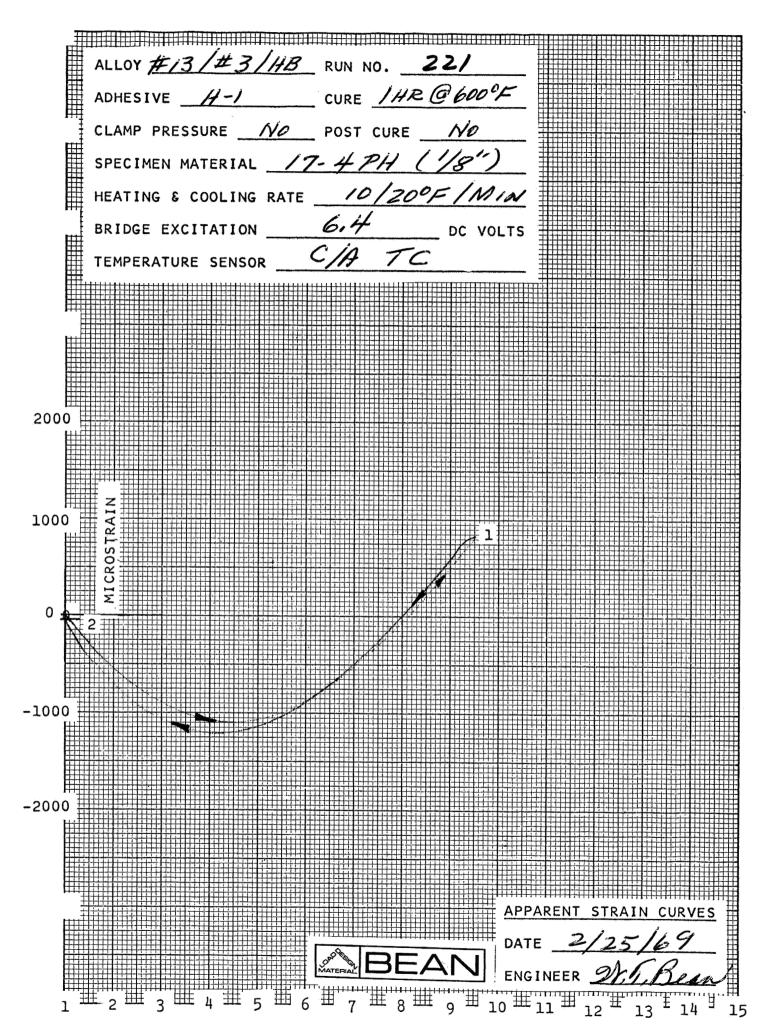


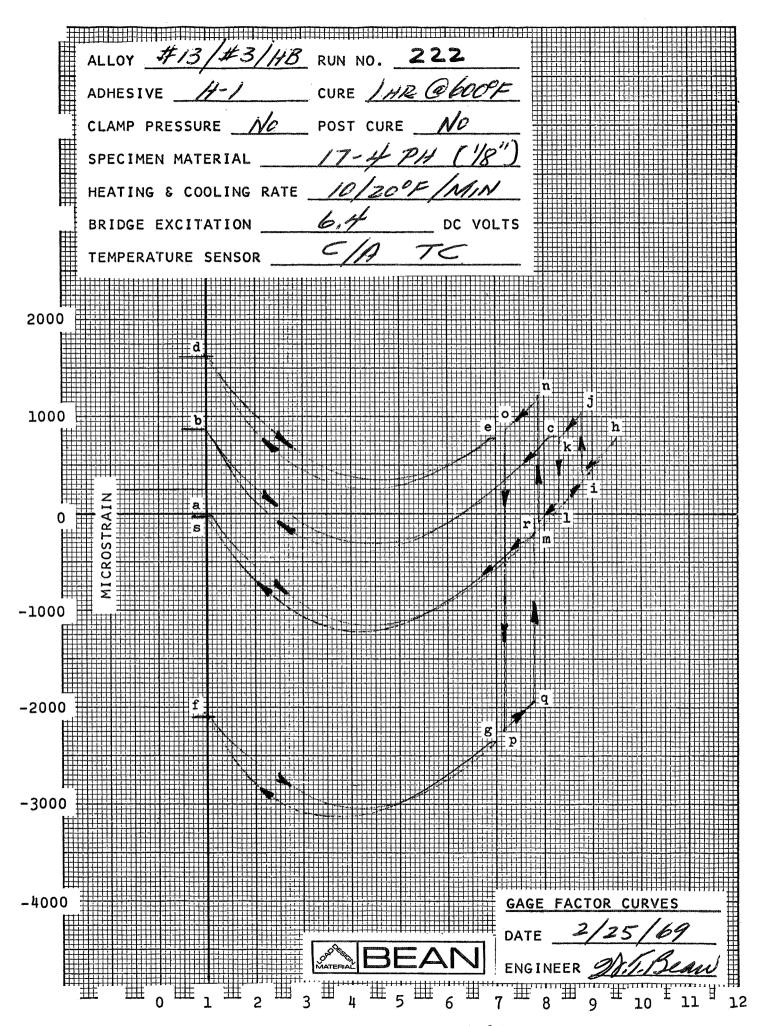


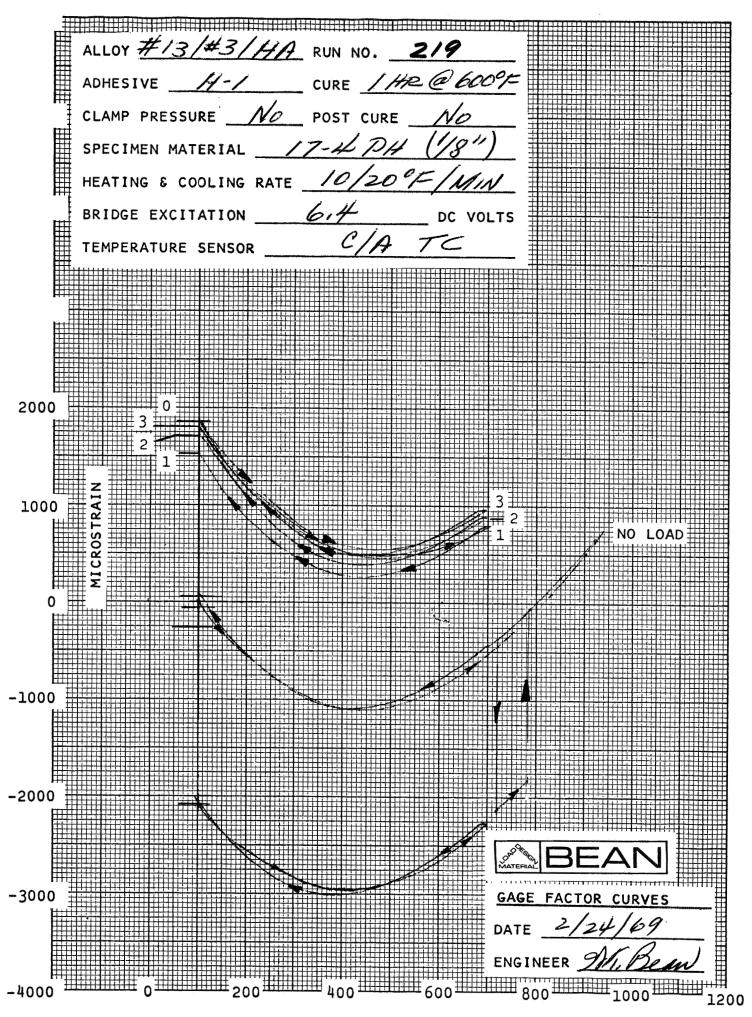


LAPSED TIME. HRS

Eraune 17







TEMPERATURE, °F

Table XI RECORD OF TEST ON J-1650 FIXTURE

RUN NO. 224, 225

TEST EVENT	DESCRIPTION OF TEST	LAPSED TIME
3-4 4-5 5-6 6-5 5-7		0:01 1:25 2:40 2:41 3:56 3:57 3:58 3:59 4:00 5:10
	New Chart (New Zero) Heat (100°F to 1200°F) no load Drift Check at 1200°F (15 min) Drift Check at 1200°F (15 min) Cool (1200°F to 100°F) no load Zero Offset (+50µɛ)	5:15 7:00 7:15 7:30 8:35 hrs



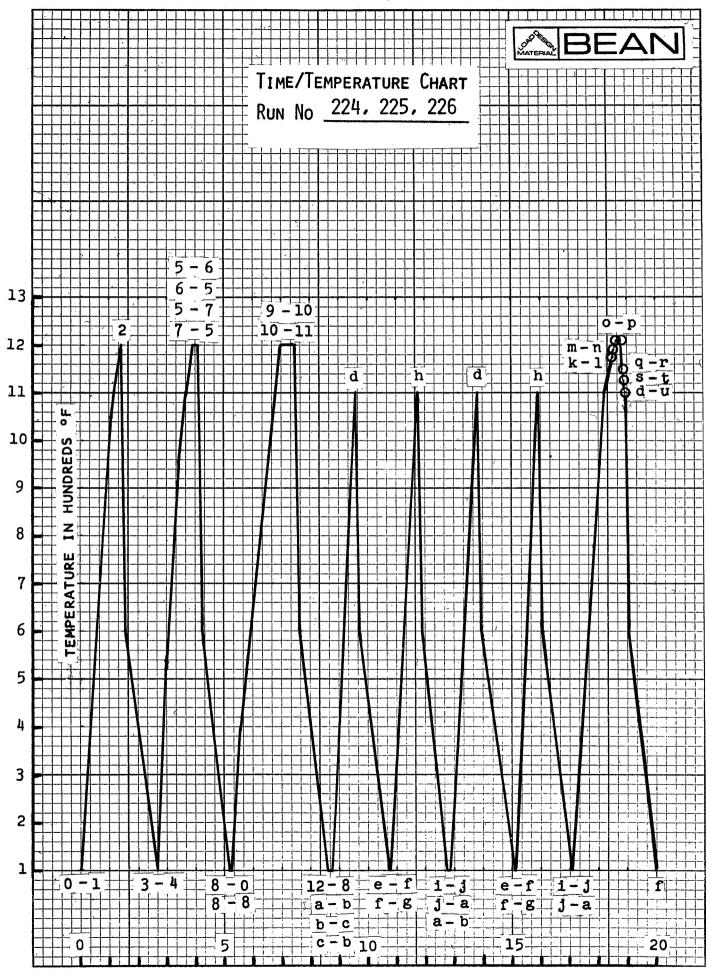
Table XII

RECORD OF TEST ON J-1650 FIXTURE

RUN NO. 226

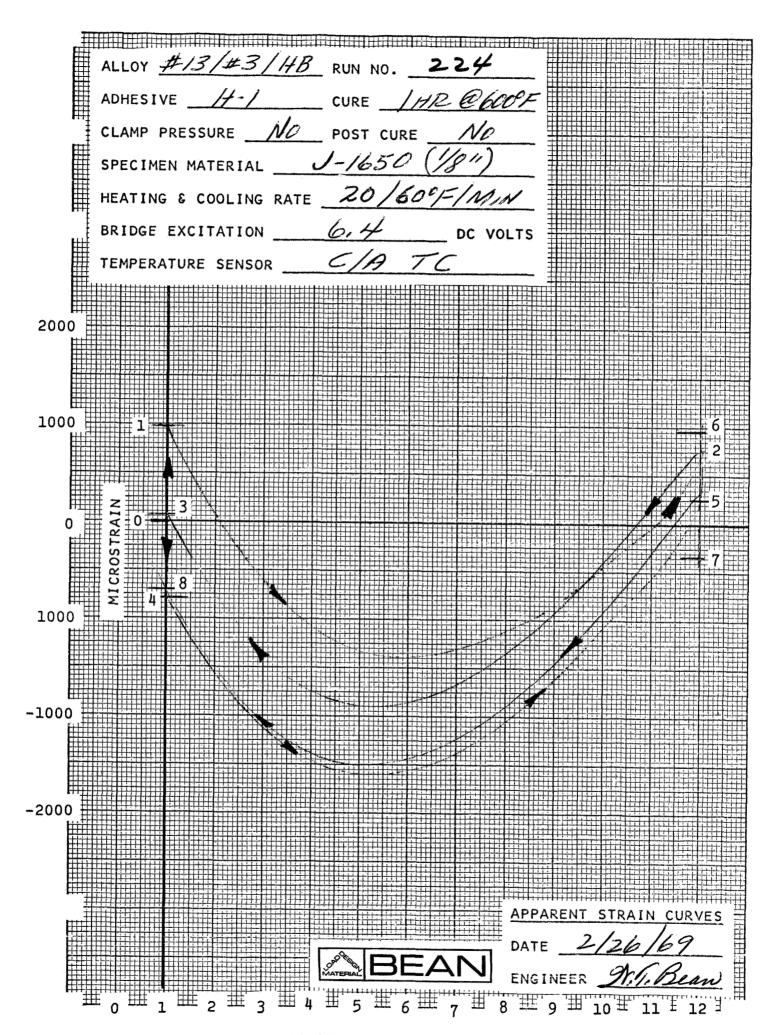
TEST EVENT	DESCRIPTION OF TEST	LAPSED TIME
a	New chart (new Zero)	8:40
a-b	Load (+990µє) 100°F	8:41
b-c	Load (-865με) 100°F	8:43
c-b	Load (+990με) 100°F	8:45
b-d	Heat (100°F to 1100°F) loaded	9:35
d-e	Cool (1100°F to 100°F) loaded	10:45
e-f	Unload "T" at 100°F	10:46
f-g	Load (-865με) 100°F	10:47
g-h	Heat (100°F to 1100°F) loaded	11:47
h-i	Cool (1100°F to 100°F) loaded	12:47
i-j	Unload "C" at 100°F	12:48
j-a	Reset Zero	12:49
a-b	Load (+990με) 100°F	12:50
b-d	Heat (100°F to 1100°F) loaded	13:50
d-e	Cool (1100°F to 100°F) loaded	15:05
e-f	Unload at 100°F "T" checks	15:06
f-g	Load (-865με) 100°F	15:07
g-h	Heat (100°F to 1100°F) loaded	15:57
h-i	Cool (1100°F to 100°F) loaded	17:02
i-j	Unload at 100°F "C" checks	17:03
j-a	Reset Zero	17:04
a-k	Heat (100°F to 1175°F) no load	18:29
k-1	Load (-815με) 1175°F	18:30
1-m	Heat (1175°F to 1190°F) loaded	18:33
m-n	Unload at 1190°F	18:34
n-o	Heat (1190°F to 1210°F) no load	18:38
o-p	Load (+960με) 1210°F	18:39
p-q	Cool (1210°F to 1150°F) loaded	18:49
q- r	Load (+960µs to -815µs) 1150°F	18:50
r-s	Cool (1150°F to 1125°F) loaded Load (-815µε to +960µε) 1125°F	18:52
s-t	Load (-815µe to +960µe) 1125°F	18:53
t-d	Cool (1125°F to 1100°F) loaded	18:55
d-u	Unload at 1100°F	18:56
u-f	Cool (1100°F to 100°F)	19:58 hrs

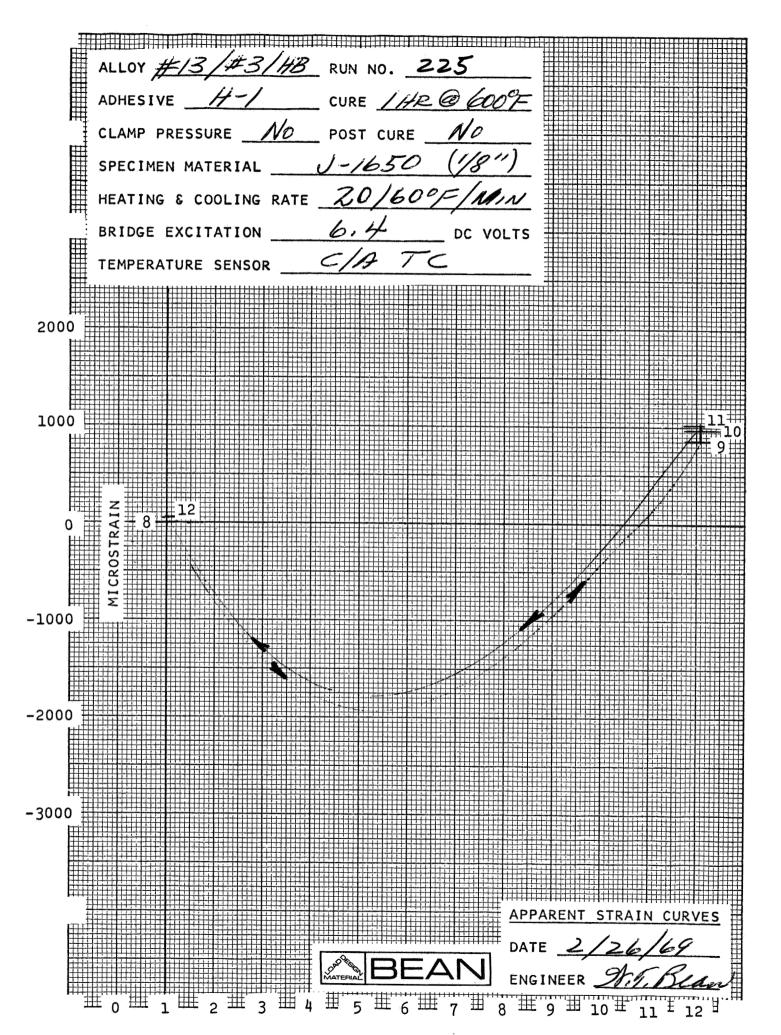


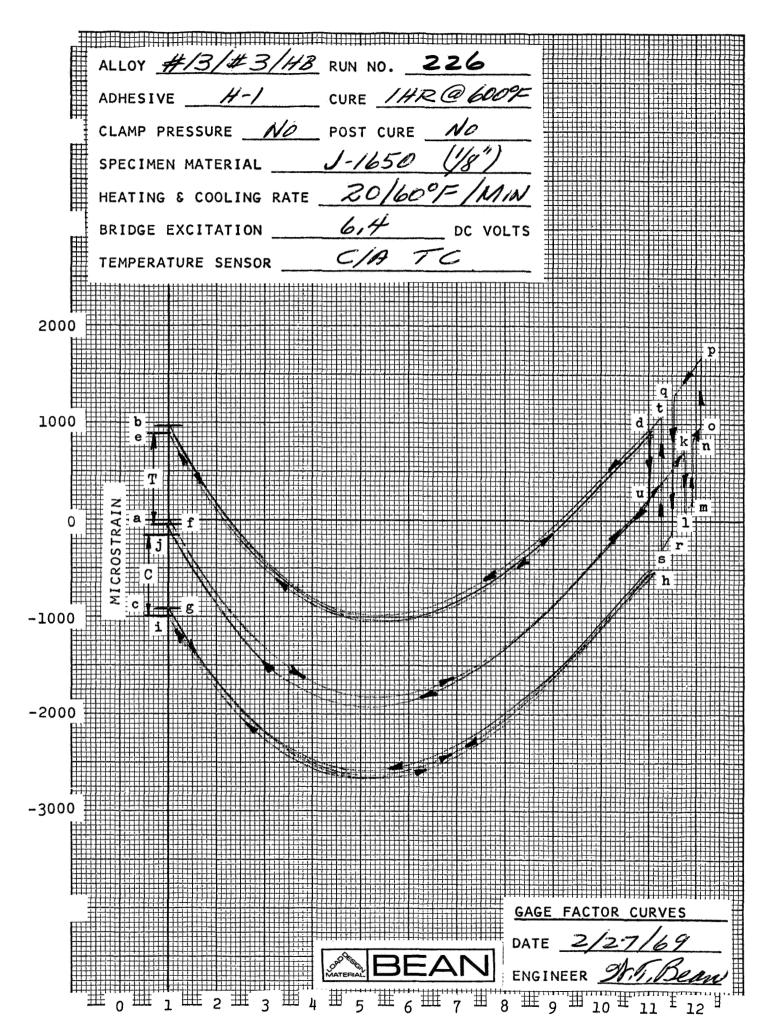


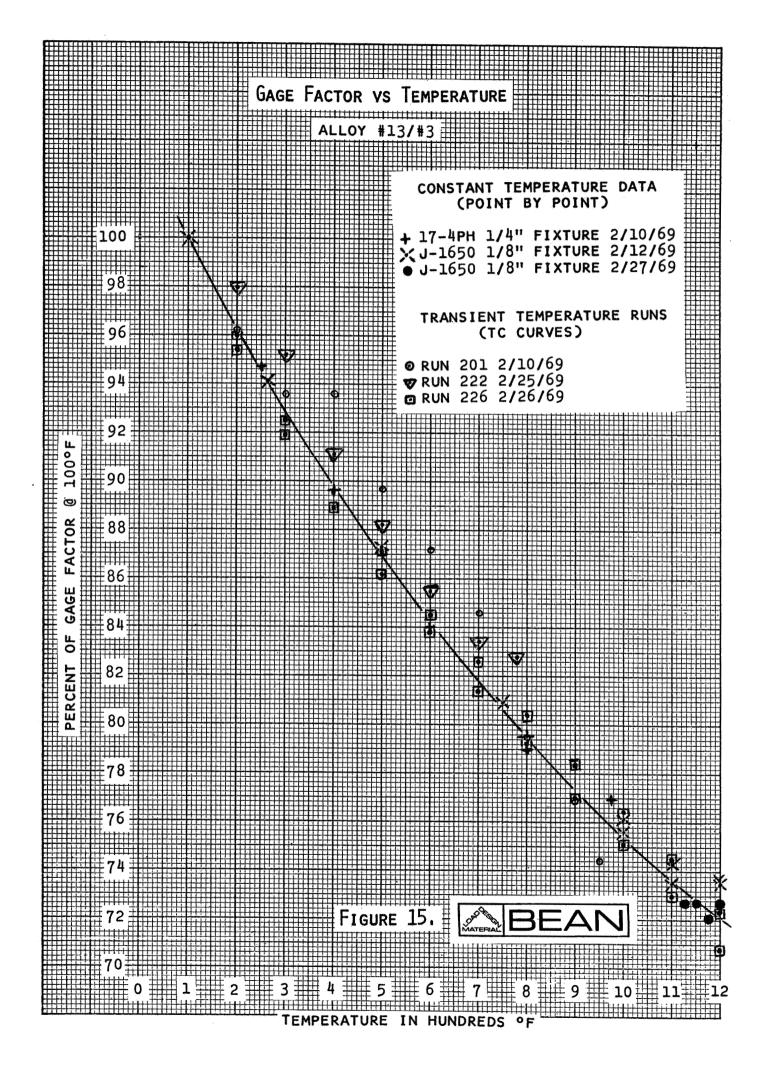
LAPSED TIME, HRS

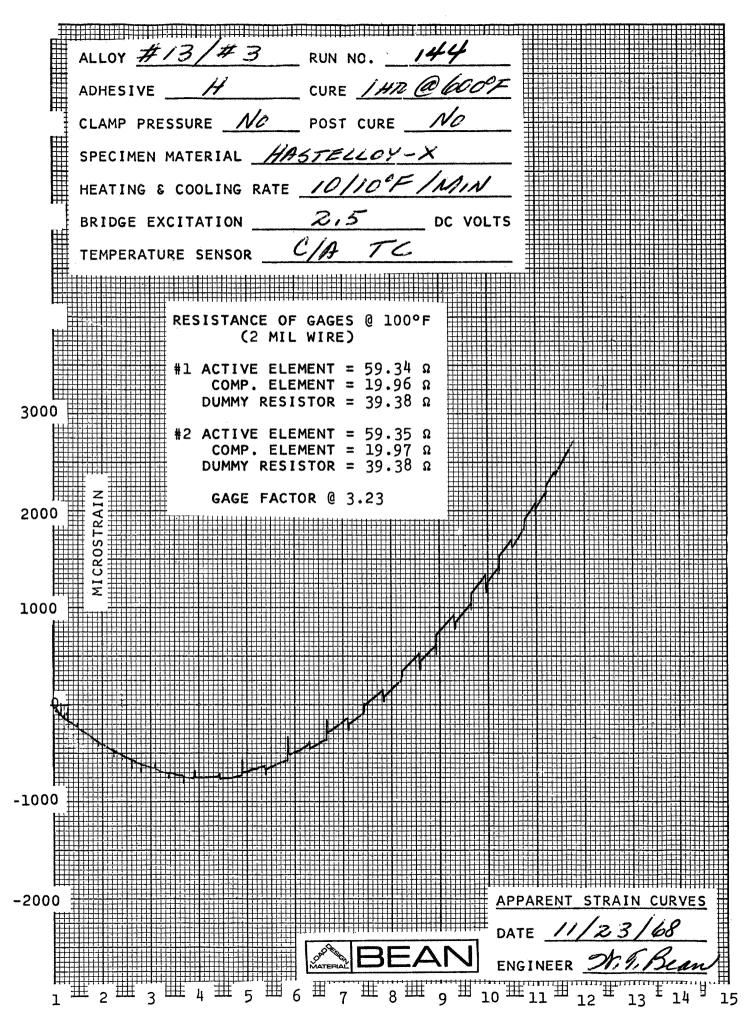
FIGURE 14.

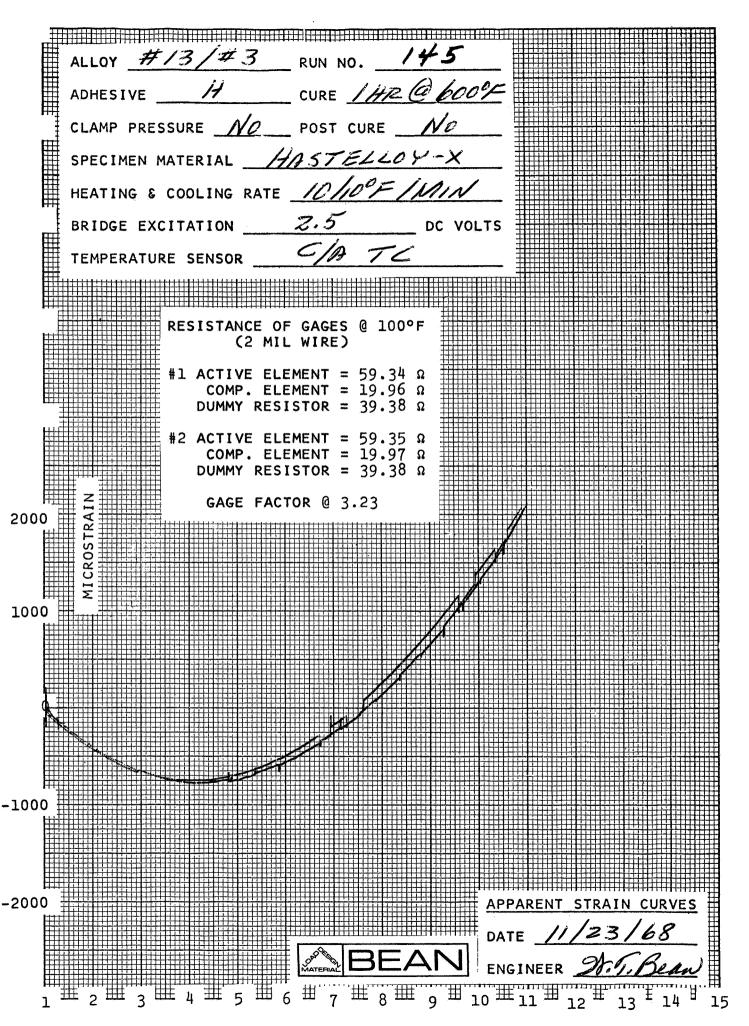


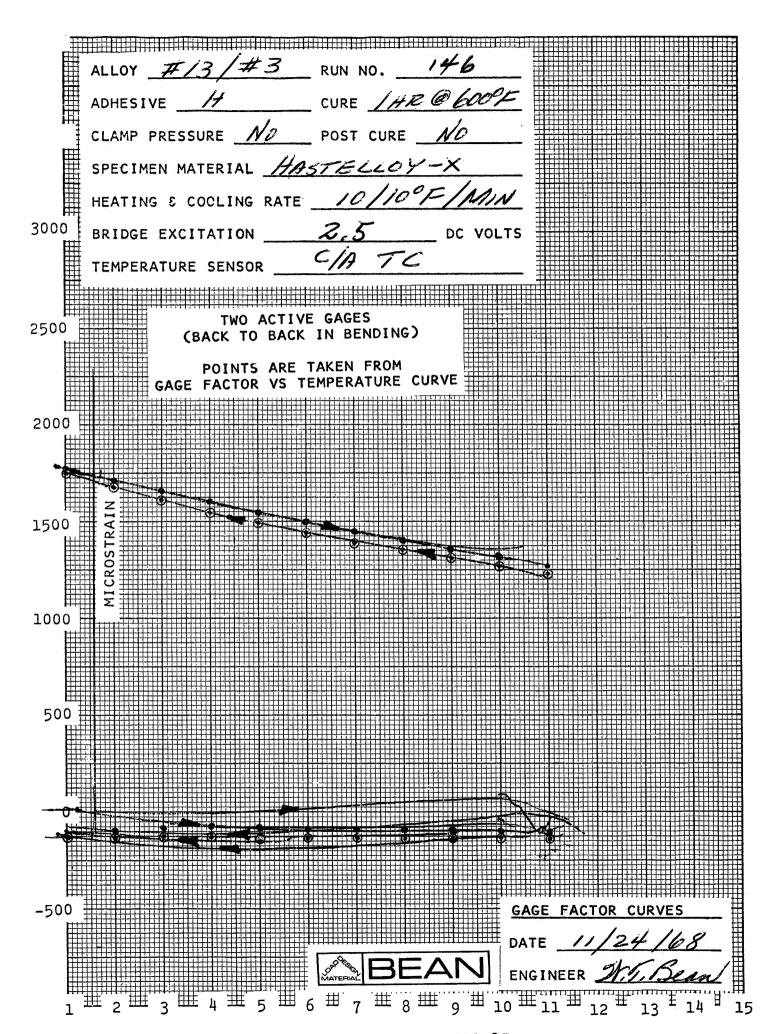


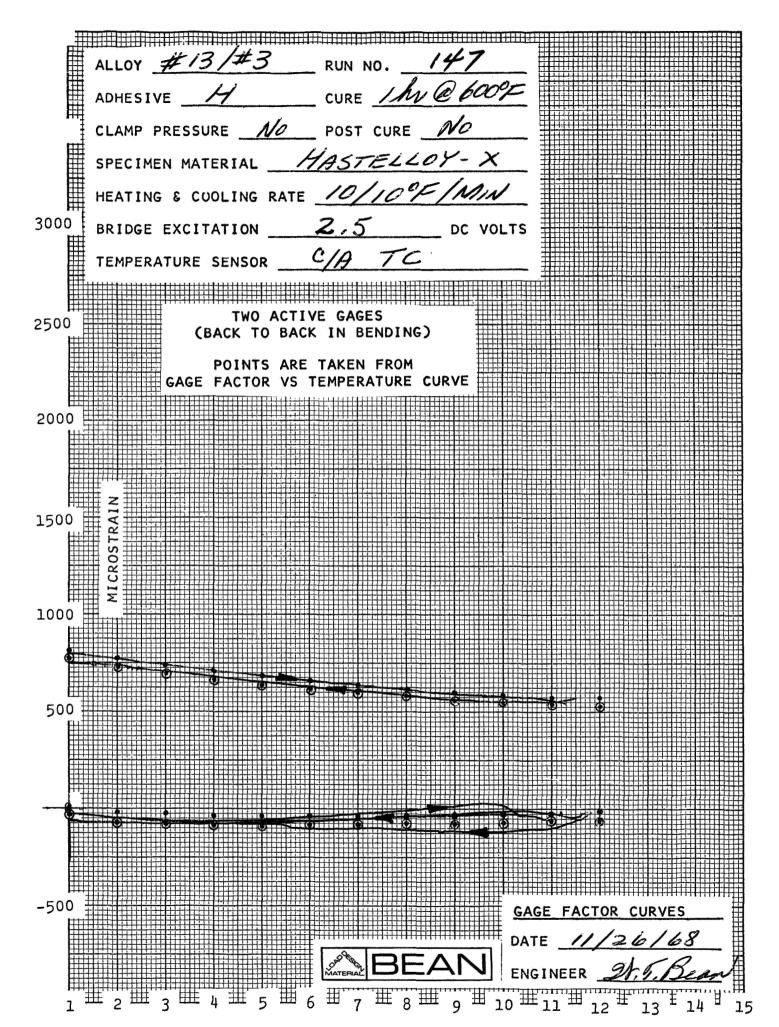






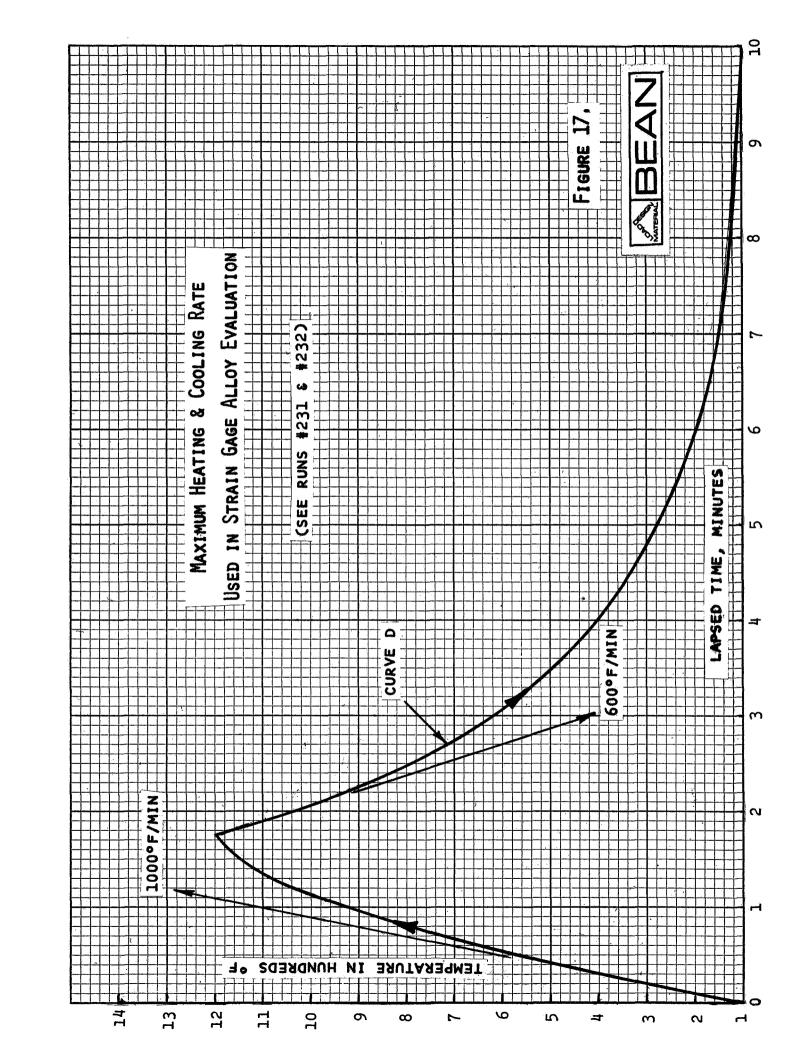


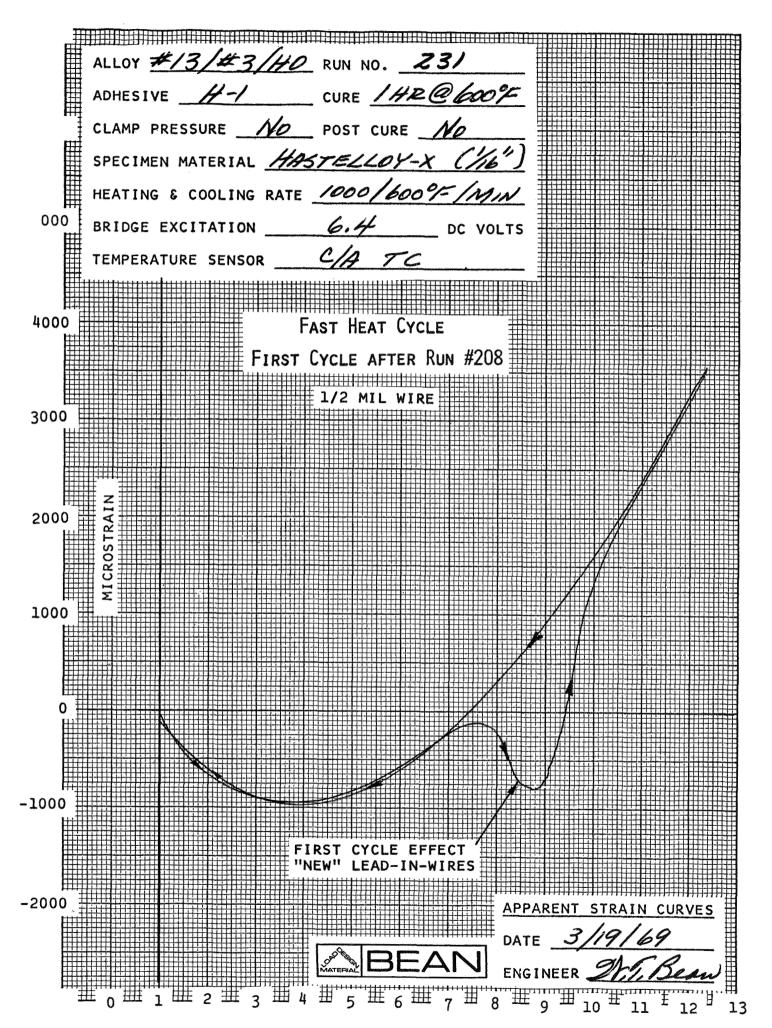


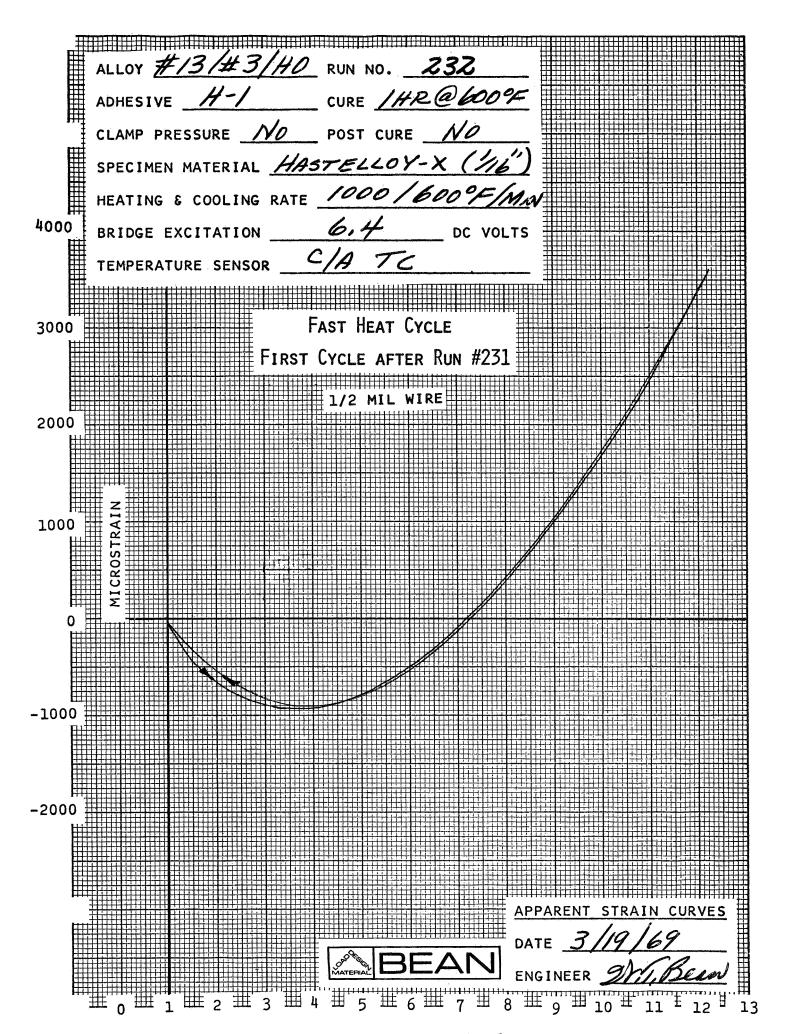


Heating and Cooling Rates

The Alloy #13/#3 gage was evaluated under various heating and cooling rates (Figures 16 and 17). Heating rates up to 1000°F per minute were employed (Runs # 231 and # 232).



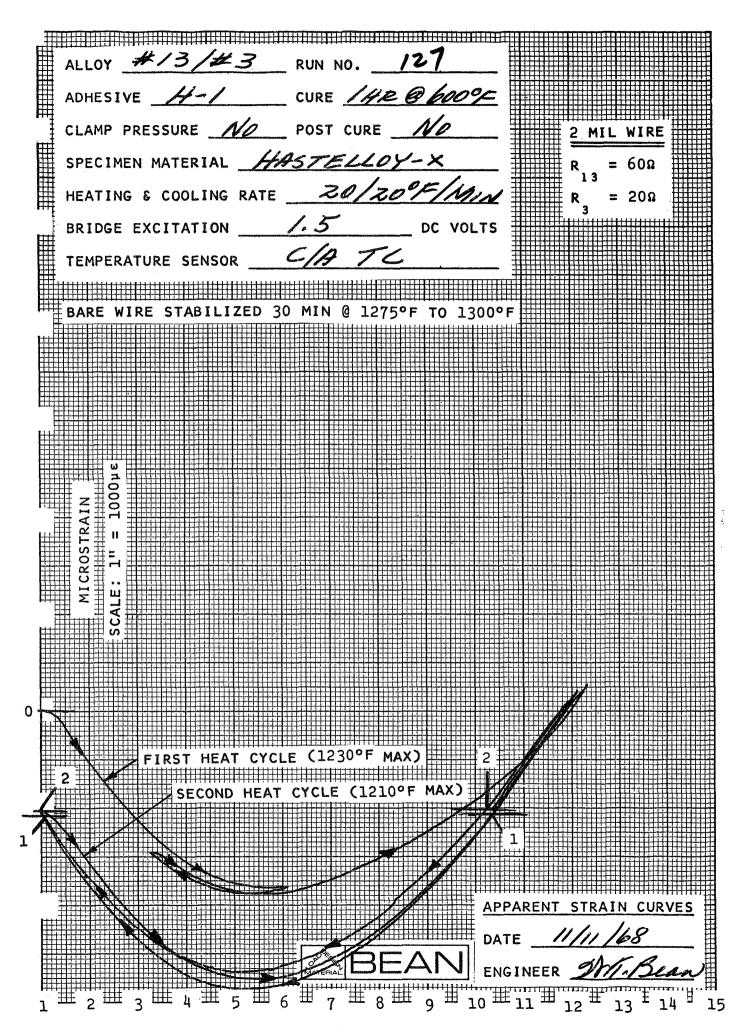




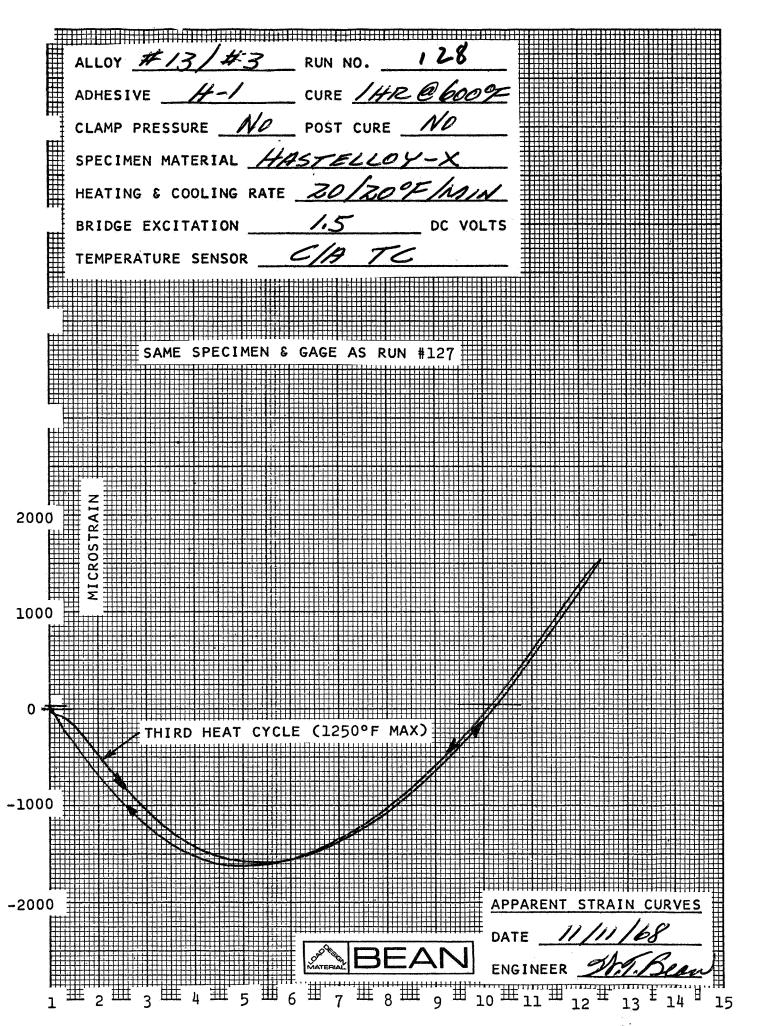
Stability

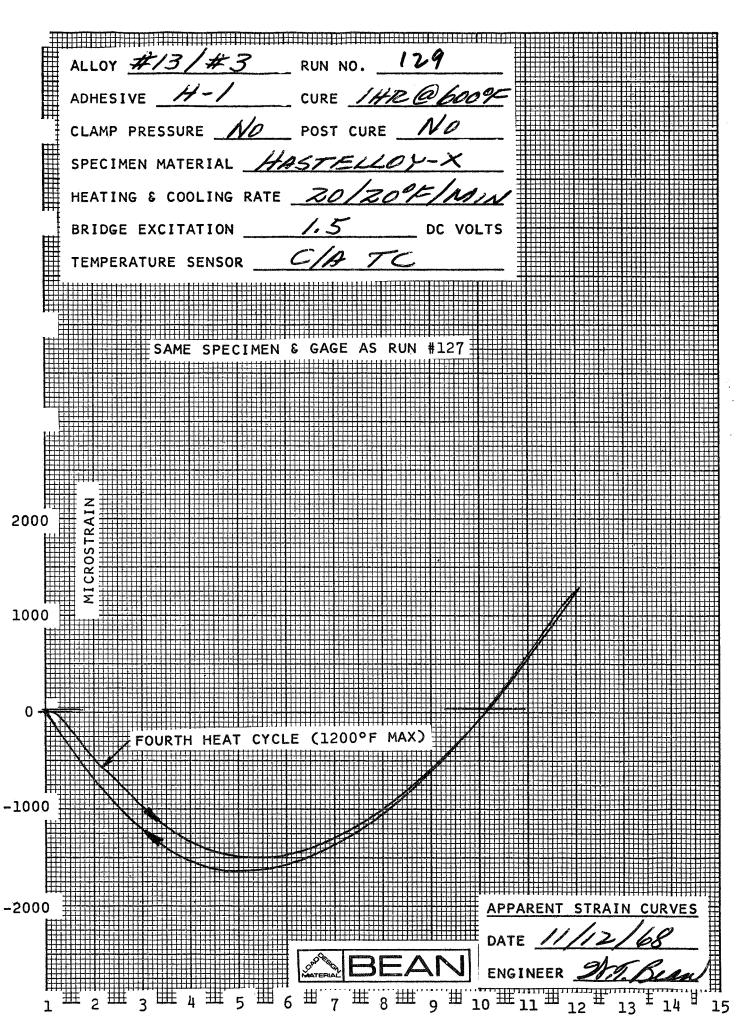
Runs # 127 through # 130 show the results of stability tests conducted on an Alloy #13/#3 strain gage. Run # 130 logged twelve hours at 1200°F. Drift at 1200°F (as well as zero offset) vs. time is indicated. Runs # 139 and # 140 show stability tests conducted on a second specimen.

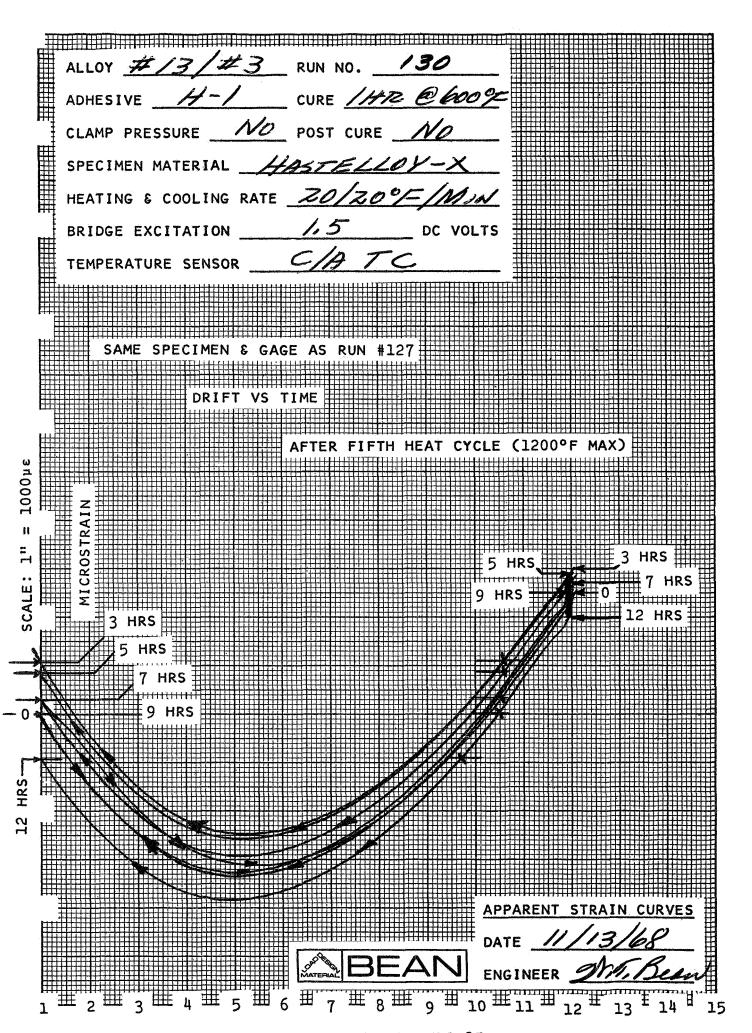
Runs # 141, # 142, # 143 show test results on a third specimen. Run # 208 was made with a strain gage employing 1/2 mil diameter wire. Figure 18 summarizes drift data.



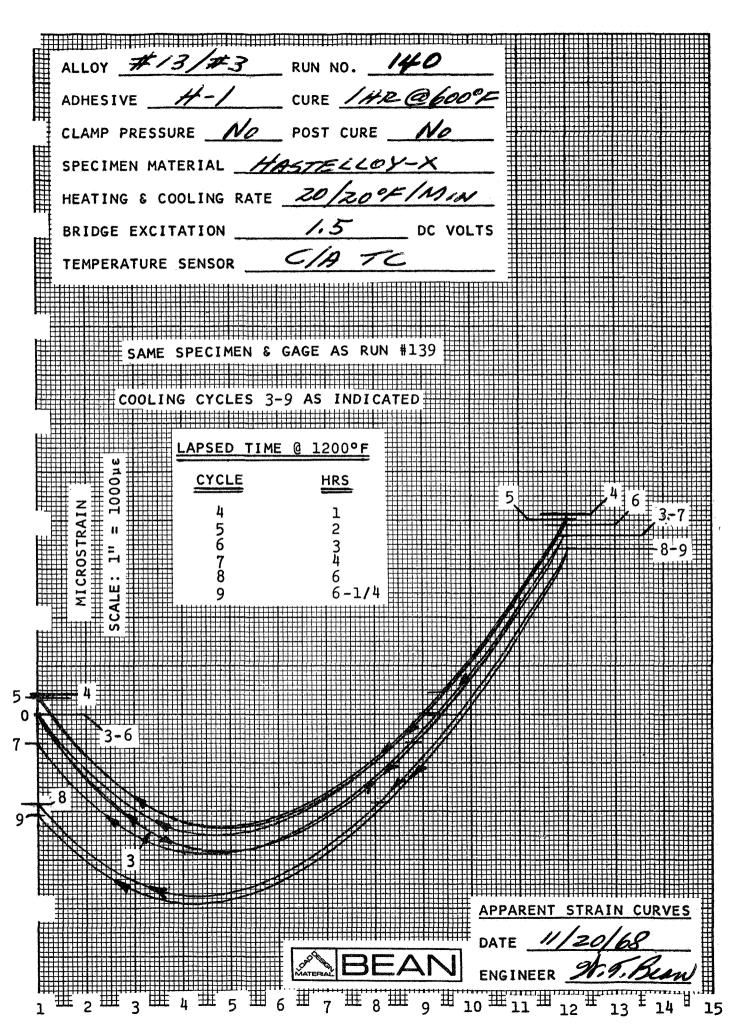
TEMPERATURE IN HUNDREDS OF



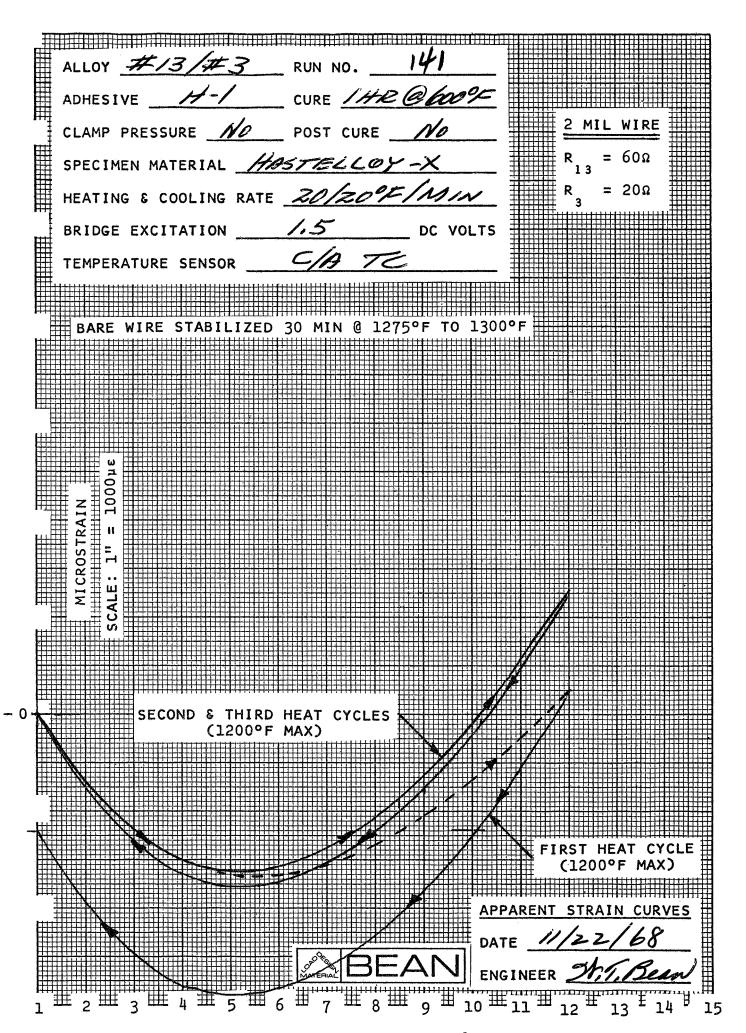


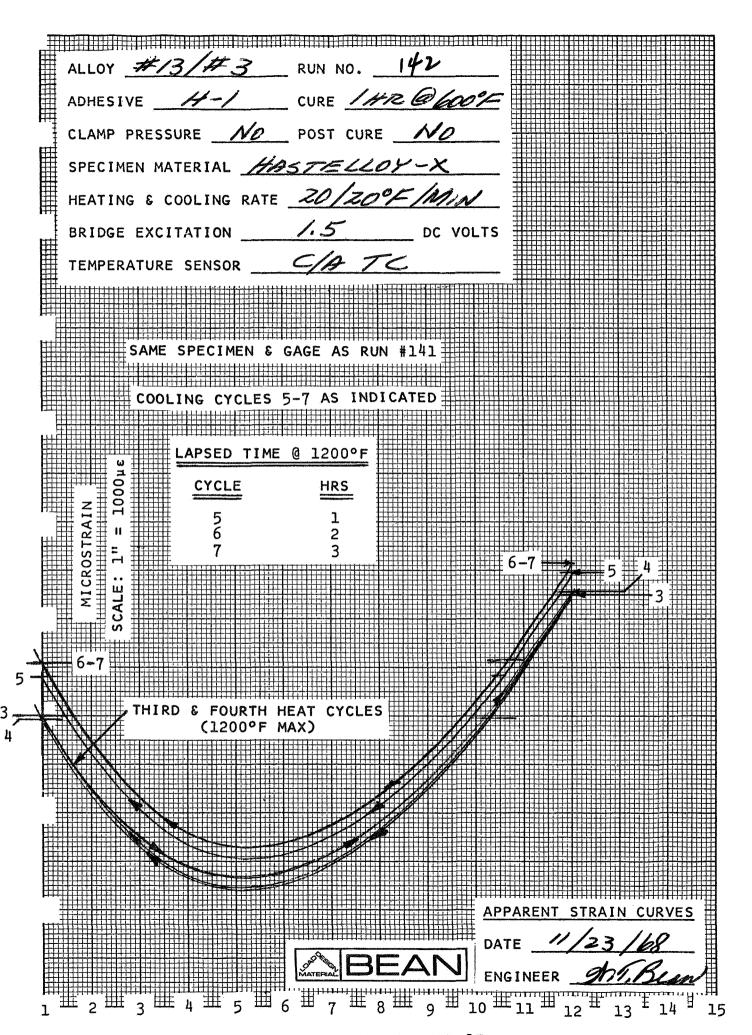


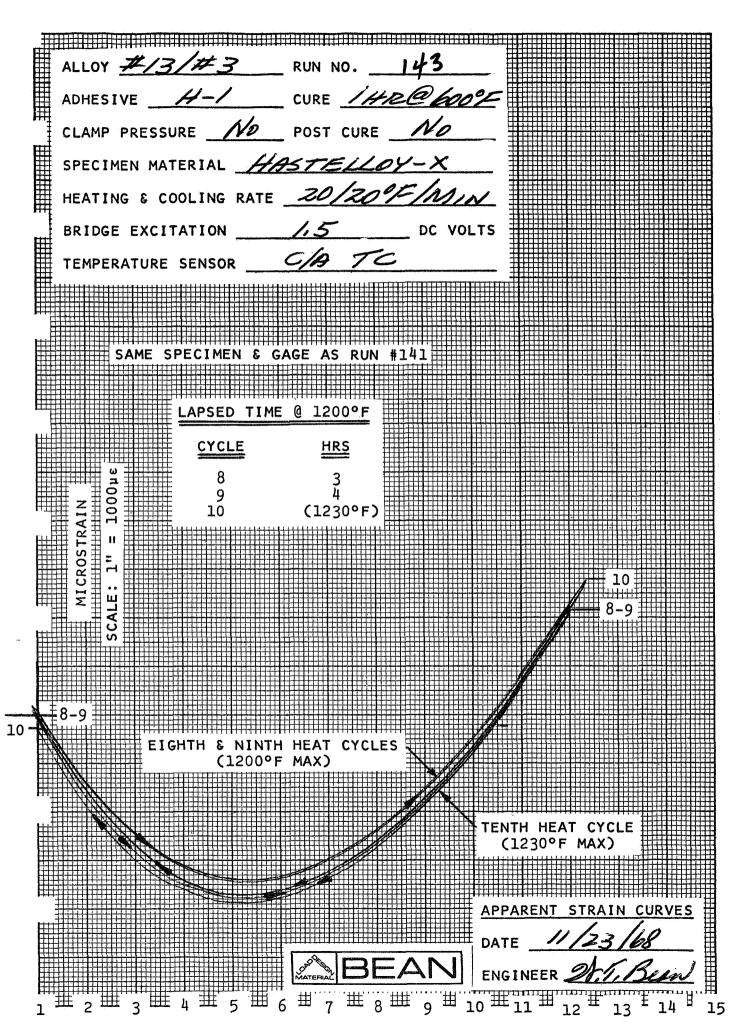
ALLOY #/3/#3 RUN NO	
ADHESIVE H-/ CURE /HR @ 60095	
CLAMP PRESSURE NO POST CURE NO	2 MIL WIRE
SPECIMEN MATERIAL HASTELLOY-X	$R_{13} = 60\Omega$
HEATING & COOLING RATE 20/2095 MIN	
BRIDGE EXCITATION DC VOLTS	3
TEMPERATURE SENSOR C/B TC	
BARE WIRE STABILIZED 30 MIN @ 1250°F TO 1275°) F
ω μ	
z	
RAI T	
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
E 1 C E :	
CAL	/
0	
FIRST HEAT CYCLE (1200°F MAX)	
	SECOND HEAT CYCLE
	(1200°F MAX)
	ARENT STRAIN CURVES
DATE	21.52
▋▘▎▘▍▎▎ ▐░▘▎▘▎▐░▎░░░░░░░░░░░░░░░░░░░░░░░░░░░░	NEER <u>IVI BLAN</u>
1 # 2 # 3 # 4 # 5 # 6 # 7 # 8 # 9 # 10 # 3	11 [#] 12 [#] 13 [‡] 14 [‡] 15



TEMPERATURE IN HUNDREDS °F







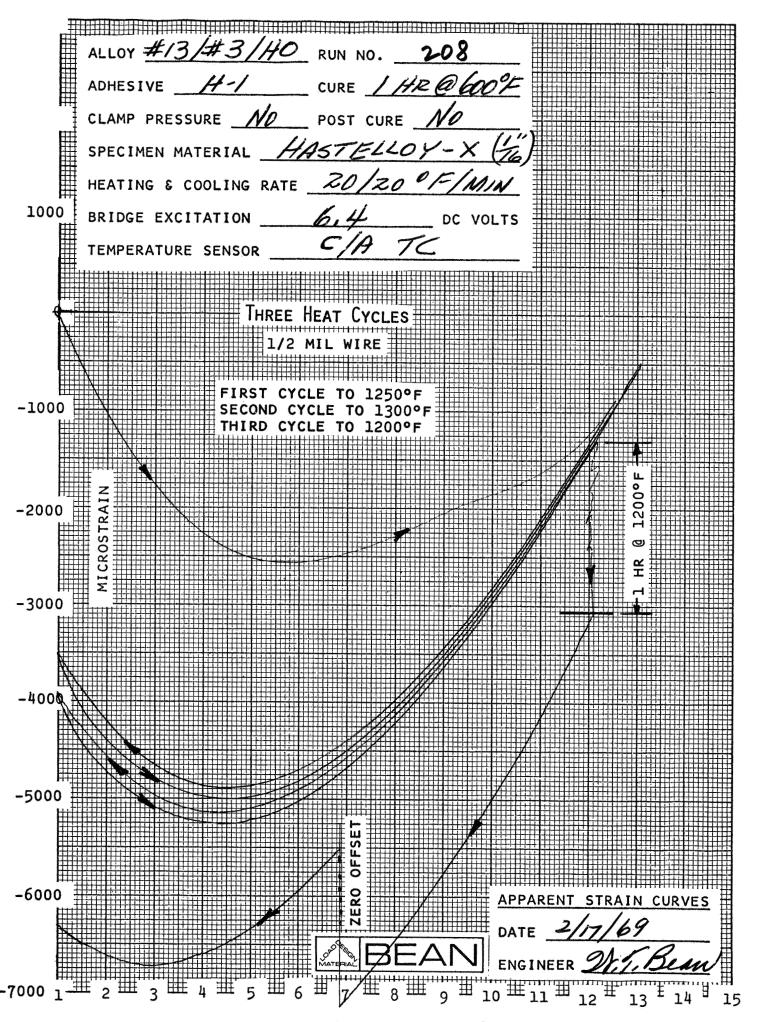


FIGURE 18.

Gage Factor vs. Strain

Several gage factor vs. strain tests were conducted by mounting the Alloy #13/#3 gage on annealed aluminum bars (1/4" x 1" x 12").

Room temperature curing epoxies, heat curing epoxies, phenolics, and ceramic adhesives were employed. A constant-moment section for the strain gage was established by the loading fixture. An annealed constantan gage was mounted on the beam for comparative purposes.

The test results are shown in Figure 19. While the gage factor decreases with increasing strain as indicated, the captive filament will yield 100% gage factor on the recovery (relaxation) cycle and subsequent cycles.

FIGURE 19.

VII. CONCLUSIONS

All "Superalloys" tested contained significant amounts of nickel and chromium and exhibited solid solution phase changes below the 1200°F operating range. A change in the solid solution results in an anomaly of the resistance vs. temperature curve and yields an unsatisfactory alloy for high-temperature strain gage usage.

Alloy # 5, however, can be considered for hightemperature dynamic work and should result in a strain gage filament superior to those currently being used in the vibratory testing of turbine blades.

Alloy #13/#3 yields a strain gage that is suitable for the measurement of steady-state strains up to 1200°F and is feasible for commercial production.

Alloy # 3 is more stable at elevated temperature than Alloy # 13.

Alloy # 4 should be evaluated as a compensating filament.

VIII. RECOMMENDATIONS

Alloys of platinum containing palladium-molybdenum should be investigated with a view toward:

- 1. Obtaining an improvement in the stability of the active filament (above 1000°F).
- 2. Achieving a more linear temperature coefficient of resistance. This will result in a more satisfactory apparent strain curve.
- 3. Increasing the coefficient of expansion in order to obtain better first cycle performance on high-expansion materials.
- 4. Reduction in gage factor. The judicious use of the proper compensating filament also would result in a more linear gage factor vs. strain.